# PhD Qualifying Examination in Acoustics 

## Closed-book

Answer all parts of at least three questions

## Problem \#1 (This problem has four parts)

a) Assume that the sound pressure level due to white noise (equal energy per unit frequency) in octave band $B$ is $L_{1}$. Find an expression for the total level for $N$ octave bands that include band $B$. Recall that the bandwidth of a given octave band is twice that of the next lowest band, that is $B W_{B}=2 \times B W_{B-1}$, where $B$ is the band number.
b) Repeat part a), except assume pink noise (equal energy per octave band).
c) An acoustic pressure signal is in the form of a periodic square wave, $p=+A$ for a time interval $T / 2$, then $p=-A$ then for a time interval $T / 2$, etc., where $A$ is constant. If the period $T$ is 0.001 seconds, and the amplitude $A$ is 1 Pa , what is the sound pressure level of this signal, dB re 20 $\mu \mathrm{Pa}$ ?
d) An acoustic pressure signal is in the form of a periodic square wave, $p=+A$ for a time interval $T / 2$, then $p=-A$ then for a time interval $T / 2$, etc., where $A$ is constant. If the period $T$ is 0.001 seconds, and the amplitude $A$ is 1 Pa , what would be the octave-band sound pressure level ( dB re $20 \mu \mathrm{~Pa}$ ) for the octave band centered at 1000 Hz ? Recall that the lower and upper band limits for octave bands are related by $\sqrt{2}$ to the center frequency of the band (i.e. $f_{\text {lower }}=f_{c} / \sqrt{2}$, $f_{\text {upper }}=f_{c} \sqrt{2}$ ).

Problem \#2 (This problem has four parts)
A circular loudspeaker of diameter 12.5 cm is mounted in a rigid baffle and driven, in air, at a frequency of 6550 Hz . Assume the speed of sound is $343 \mathrm{~m} / \mathrm{s}$, and $\rho c=400$ Rayl.
a) Find the Rayleigh distance
b) How much acoustic power ( mW ) is radiated when the sound pressure level on axis is 93 dB at a distance of 1 m ?
b) Find the half-power beamwidth (in the farfield)
d) Find the location of the most distant null on the axis

Work these problems as far as you can; clearly state all assumptions or approximations, and if possible, validate your approximations. You will receive full credit if your final expression(s) merely lack numerical evaluation.
$p(x, y, z, t)=\frac{j k \rho_{o} c_{o} u_{o} e^{j \omega t}}{2 \pi} \int_{S} \frac{e^{-j k R}}{R} d S$
$p(r, \theta, t)=\frac{j a \rho_{o} c_{o} u_{o} e^{j \omega t}}{r} \frac{k a}{2} e^{j(\omega t-k r)}$
$p=P_{0}\left[e^{j(\omega t-k r)}-e^{j\left(\omega t-k_{1}\right)}\right]$
$D(\theta)=\frac{2 J_{1}(k a \sin \theta)}{k a \sin \theta}$
$\frac{2 J_{1}(k a \sin \theta)}{k a \sin \theta}=\frac{1}{\sqrt{2}}$
$2 \theta=2 \sin ^{-1}(1.616 / k a)$
$W=S u_{r m s}^{2} \operatorname{Re}\left(Z_{p}\right)$
$R_{1}(2 k a)=1-\frac{2 J_{1}(2 k a)}{2 k a}$
$W=\frac{\pi a^{2}}{2 \rho c} P_{0}^{2} R_{1}(2 k a)$
$R_{0}=S / \lambda=k a^{2} / 2$
$p=\frac{P_{0} R_{0}}{r} e^{j\left(\omega t-k\left(r-R_{0}\right)\right)}$
$\sin \left(\pi a / \lambda\left(\sqrt{(a / r)^{2}+1}-(a / r)\right)\right)=0$

## A6 TABLE OF DIRECTIVITIES AND IMPEDANCE FUNCTIONS FOR A PISTON

| $x$ | Directivity Functions$(x=k a \sin \theta)$ |  | Impedance Functions$(x=2 k a)$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Pressure | Intensity | Resistance | Resistance |
|  | $\frac{2 J_{1}(x)}{x}$ | $\left(\frac{2 J_{1}(x)}{x}\right)^{2}$ | $R_{1}(x)$ | $X_{1}(x)$ |
| 0.0 | 1.0000 | 1.0000 | 0.0000 | 0.0000 |
| 0.2 | 0.9950 | 0.9900 | 0.0050 | 0.0847 |
| 0.4 | 0.9802 | 0.9608 | 0.0198 | 0.1680 |
| 0.6 | 0.9557 | 0.9134 | 0.0443 | 0.2486 |
| 0.8 | 0.9221 | 0.8503 | 0.0779 | 0.3253 |
| 1.0 | 0.8801 | 0.7746 | 0.1199 | 0.3969 |
| 1.2 | 0.8305 | 0.6897 | 0.1695 | 0.4624 |
| 1.4 | 0.7743 | 0.5995 | 0.2257 | 0.5207 |
| 1.6 | 0.7124 | 0.5075 | 0.2876 | 0.5713 |
| 1.8 | 0.6461 | 0.4174 | 0.3539 | 0.6134 |
| 2.0 | 0.5767 | 0.3326 | 0.4233 | 0.6468 |
| 2.2 | 0.5054 | 0.2554 | 0.4946 | 0.6711 |
| 2.4 | 0.4335 | 0.1879 | 0.5665 | 0.6862 |
| 2.6 | 0.3622 | 0.1326 | 0.6378 | 0.6925 |
| 2.8 | 0.2927 | 0.0857 | 0.7073 | 0.6903 |
| 3.0 | 0.2260 | 0.0511 | 0.7740 | 0.6800 |
| 3.2 | 0.1633 | 0.0267 | 0.8367 | 0.6623 |
| 3.4 | 0.1054 | 0.0111 | 0.8946 | 0.6381 |
| 3.6 | 0.0530 | 0.0028 | 0.9470 | 0.6081 |
| 3.8 | +0.0068 | 0.00005 | 0.9932 | 0.5733 |
| 4.0 | $-0.0330$ | 0.0011 | 1.0330 | 0.5349 |
| 4.5 | -0.1027 | 0.0104 | 1.1027 | 0.4293 |
| 5.0 | -0.1310 | 0.0172 | 1.1310 | 0.3232 |
| 5.5 | -0.1242 | 0.0154 | 1.1242 | 0.2299 |
| 6.0 | -0.0922 | 0.0085 | 1.0922 | 0.1594 |
| 6.5 | -0.0473 | 0.0022 | 1.0473 | 0.1159 |
| 7.0 | -0.0013 | 0.00000 | 1.0013 | 0.0989 |
| 7.5 | +0.0361 | 0.0013 | 0.9639 | 0.1036 |
| 8.0 | 0.0587 | 0.0034 | 0.9413 | 0.1219 |
| 8.5 | 0.0643 | 0.0041 | 0.9357 | 0.1457 |
| 9.0 | 0.0545 | 0.0030 | 0.9455 | 0.1663 |
| 9.5 | 0.0339 | 0.0011 | 0.9661 | 0.1782 |
| 10.0 | $+0.0087$ | 0.00008 | 0.9913 | 0.1784 |
| 10.5 | $-0.0150$ | 0.0002 | 1.0150 | 0.1668 |
| 11.0 | -0.0321 | 0.0010 | 1.0321 | 0.1464 |
| 11.5 | -0.0397 | 0.0016 | 1.0397 | 0.1216 |
| 12.0 | -0.0372 | 0.0014 | 1.0372 | 0.0973 |
| 12.5 | -0.0265 | 0.0007 | 1.0265 | 0.0779 |
| 13.0 | -0.0108 | 0.0001 | 1.0108 | 0.0662 |
| 13.5 | $+0.0056$ | 0.00003 | 0.9944 | 0.0631 |
| 14.0 | 0.0191 | 0.0004 | 0.9809 | 0.0676 |
| 14.5 | 0.0267 | 0.0007 | 0.9733 | 0.0770 |
| 15.0 | 0.0273 | 0.0007 | 0.9727 | 0.0880 |
| 15.5 | 0.0216 | 0.0005 | 0.9784 | 0.0973 |
| 16.0 | 0.0113 | 0.0001 | 0.9887 | 0.1021 |

## Problem \#3 (This problem has two parts)

1) In many applications of acoustics the ambient fluid is not motionless. The simplest extension of the motionless-ambient-fluid formulation of acoustics, involves ambient fluid motion at a constant velocity $\vec{U}$ where $\vec{U}=U_{x} \hat{x}+U_{y} \hat{y}+U_{z} \hat{z}$ is a constant vector in both time and space. Under this assumption, demonstrate that the linearized acoustic wave equation in air for the pressure fluctuation $p$ can be expressed as

$$
\left[\frac{\partial}{\partial}+\vec{U} \cdot \vec{\nabla}\right]\left[\frac{\partial}{\partial}+\vec{U} \cdot \vec{\nabla}\right] p-c^{2} \nabla^{2} p=0 \quad \text { Eq. (1) }
$$

starting from

- the continuity equation: $\frac{\partial \rho}{\partial}+\vec{\nabla} \cdot(\rho \vec{u})=0$
- Euler's ideal flow momentum equation:

$$
\frac{\partial \vec{u}}{\partial t}+(\vec{u} \cdot \vec{\nabla}) \vec{\mu}+\frac{1}{\rho} \vec{\nabla} P=0
$$

- the constitutive equation: $\rho=\rho_{o}+p / c^{2}$
where $\rho$ is the total density, $\vec{u}$ the total velocity of the fluid and $\rho_{o}$ is reference density in absence of acoustic wave.

Assume that $\vec{U}=U_{x} \hat{x}+U_{y} \hat{y}+U_{z} \hat{z}$ is a constant vector in both time and space. Also Assume that the speed of sound, $c$, ambient static pressure $P_{o}$ and reference density $\rho_{o}$ are independent of time and constant everywhere.
[Hint. The gradient operator, $\vec{\nabla}=\hat{x} \frac{\partial}{\partial x}+\hat{y} \frac{\partial}{\partial y}+\hat{z} \frac{\partial}{\partial z}$ in Cartesian coordinates, is merely a short hand notation for a vector derivative. It follows all the usual rules for differentiation except that it also has a vector character, so the order of dot-products needs to be respected, for example:

$$
\left.\vec{U} \cdot \vec{\nabla}=U_{x} \frac{\partial}{\partial x}+U_{y} \frac{\partial}{\partial y}+U_{z} \frac{\partial}{\partial z} \neq \vec{\nabla} \cdot \vec{U}=\frac{\partial U_{x}}{\partial x}+\frac{\partial U_{y}}{\partial y}+\frac{\partial U_{z}}{\partial z} .\right]
$$

2) Obtain the dispersion relationship between the wavenumber $k$ and the frequency $\omega$ for a harmonic plane wave solution of Eq. (1) and propagating along the $x$ direction only. Assume $\vec{U}=U_{x} \hat{X}$.

## Problem \#4 (This problem has three parts)

A plane wave of frequency $\omega$ is normally incident on the boundary between two fluids of characteristic impedance $r_{1}$ and $r_{3}$ (Fig. a). The fluid densities of the fluids are $\rho_{1}$ and $\rho_{3}$. Assume that $\mathrm{r}_{3}=0.01 \mathrm{r}_{1}$.
a.

b.

(1) For the configuration in Fig. a, calculate the pressure transmission coefficient, T, and the intensity transmission coefficient $\mathrm{T}_{\mathrm{I}}$ (2points)
(2) In order to increase the transmission of power at specific frequencies, a layer of thickness L is added between fluids 1 and 3 (Fig. b). This layer is made of a material of characteristic impedance $r_{2}$ and density $\rho_{2}$. Write a system of equations that need to be solved in order to find the pressure reflection coefficient and the pressure transmission coefficient. Clearly write the unknowns in the equations; the other terms should be expressed as a function of the given parameters. (3 points)
(3) If we solve this system of equations from part 2, we obtain the following expression for the pressure reflection coefficient:

$$
R=\frac{\left(1-r_{1} / r_{3}\right) \cos k_{2} L+j\left(r_{2} / r_{3}-r_{1} / r_{2}\right) \sin k_{2} L}{\left(1+r_{1} / r_{3}\right) \cos k_{2} L+j\left(r_{2} / r_{3}+r_{1} / r_{2}\right) \sin k_{2} L}
$$

If $E=\frac{\pi}{2 \pi_{\mathrm{a}}}$, calculate the intensity transmission coefficient $\mathrm{T}_{\mathrm{I}}$. Determine the value of $\mathrm{r}_{2}$ that maximize the transmission of acoustic energy and the maximum value of $\mathrm{T}_{\mathrm{I}}$. (5 points)

