

DEC 12 1998

RESERVE DESK

GEORGIA INSTITUTE OF TECHNOLOGY

The George W. Woodruff School of Mechanical Engineering

Nuclear Engineering

Ph.D. Qualifying Exam

Fall Quarter, 1998

Day 1

Instructions

Your Code No.: _____

- 1. Complete one of each subject, for a total of 7* completed questions.**
- 2. Use a separate page for each answer sheet (no front to back answers).**
- 3. Put **your code** on each of your answer sheets.**
- 4. The question number should be shown on each answer sheet.**
- 5. Staple your question sheet to your answer sheets and turn in.**

***Do NOT do more than 7 problems. If more than the requested number of problems are answered, then only the first 7 with the least scores will be counted towards the total score.**

Day 1

Math

1. Given

$$\frac{d^2y}{dx^2} - a^2y = \alpha \quad y(0) = 0 \quad \left. \frac{dy}{dx} \right|_{x=0} = 1,$$

Solve for y .

Day 1

Math

2. Solve the one-group diffusion equation for the neutron flux distribution within a slab subcritical multiplying medium of thickness L with an incident current of $J(\#/m^2\text{-s})$ on one surface and a 'zero flux' boundary condition on the other surface.

Day 1

Basic Fission

3. Write down the one-speed, steady-state neutron diffusion equation and give a physical description for each of the terms.



Day 1

Basic Fission

4. Explain what is meant by a 'critical' nuclear reactor. Write a one-group equation describing the 'criticality condition' for a bare cube reactor of dimension L on a side. Define the physical meaning of all terms.



Day 1**Fusion**

5. Describe the D-T fusion fuel cycle. What are the reaction products of the D-T reaction? How much energy is liberated and in what form? How is the D and T 'fuel' produced? Write any reaction equations involved.

Day 1

Fusion

6. Describe the principles of magnetic confinement of a plasma. Write an equation describing the basic force law for charged particles moving in a magnetic field and discuss the implications of the solution of this equation for plasma confinement. Explain how a plasma is confined in a tokamak.

Day 1

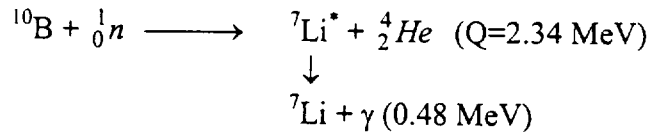
Nuclear Physics

7. A 1-MeV neutron undergoes an elastic scattering with a hydrogen nucleus. Assume that the scattering is isotropic in the center-of-mass system, calculate:
- the percentage of scattered neutron that are forwardly directed (i.e. with the scattering angle less than 90° in the lab system),
 - the energy of scattered neutron for a scattering angle of 45° in the lab system.



Day 1**Nuclear Physics**

8. A 0.48-MeV prompt gamma photon is emitted from the ${}^7\text{Li}^*$ ion in the following thermal neutron capture reaction:



Because the ${}^7\text{Li}^*$ ion travels at a relatively fast speed while emitting the gamma photon, the Doppler effect is expected for the observed gamma photon energy. That is, the observed gamma photons will not be monoenergetic at 0.48 MeV. Instead, the photon energy will spread over a range. Calculate the energy range of the observed gamma photons.



Day 1**Radiation Detection**

9. A 2"-dia. spherical ^3He proportional counter is placed in a broad/uniform neutron beam to measure the thermal neutron fluence rate ($\text{neutrons}\cdot\text{cm}^{-2}\cdot\text{sec}^{-1}$). The gas pressure in the counter is 10 atm. Given that the counter measures a total of 1,000 counts in 10 minutes and that the background count rate is 10 ± 0.2 counts/min, estimate the thermal neutron fluence rate (including uncertainty) of the beam. Data: σ_{th} for ^3He is 5400 barns.

Day 1

Radiation Detection

10. You are asked to put together a neutron detection system to perform time-of-flight (TOF) measurement of a fast neutron beam.
What kind of detector will you use?
Why?
How are you going to obtain the neutron energy information from the TOF measurement?
Also, please draw a schematic diagram of the detection system.

Day 1**Thermodynamics and Mechanics**

11. An ideal gas is initially in a piston-cylinder system with $P_1 = 150$ kPa pressure, $T_1 = 50^\circ\text{C}$ temperature and $V_1 = 0.03$ m³ volume. The system is first heated at constant pressure until the volume doubles. It is then allowed to expand isothermally until its volume doubles again.
- Calculate the total work done by the gas.
 - Find the final pressure and temperature of the gas.
 - Calculate the total heat added to the system if the gas is nitrogen.

For nitrogen assume:

$$C_p = 1.05 \text{ kJ/kg K}$$

$$C_v = 0.759 \text{ kJ/kg K}$$

$$R = 296.8 \text{ Nm/kg K}$$

Day 1

Thermodynamics and Mechanics

12. A two-loop 1600 MWt PWR is operating steadily at full power. The pressurizer contains 600 ft³ of saturated liquid and 400 ft³ of saturated vapor at 2200 psia. A steam line break occurred resulting in rapid cool down and pressure reduction in the primary system.
- a. Determine the amount of pressurizer out surge (lb_m) from event initiation until the reactor trips at a primary system pressure of 1900 psia. Assume that the pressurizer heaters will not be activated.

(Table attached)



Table 2: Saturated Steam: Pressure Table

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Abs Press. Lb/Sq In. <i>p</i>	Temp Fahr <i>t</i>	Specific Volume			Enthalpy			Entropy			Abs Press. Lb/Sq In. <i>p</i>
		Sat. Liquid <i>v_f</i>	Evap <i>v_{fg}</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>h_f</i>	Evap <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Evap <i>s_{fg}</i>	Sat. Vapor <i>s_g</i>	
0.02005	32.018	0.016022	2302.4	2302.4	0.0003	1075.5	1075.5	0.0000	2.1872	2.1872	0.02005
0.25	59.323	0.016032	2235.5	2235.5	27.382	1060.1	1087.4	0.0542	2.0425	2.0967	0.25
0.50	79.586	0.016071	2141.5	2141.5	47.623	1048.6	1096.3	0.0925	1.9446	2.0370	0.50
1.0	101.74	0.016136	2033.59	2033.59	69.73	1036.9	1105.8	0.1326	1.8455	1.9781	1.0
5.0	162.24	0.016407	17515	17515	130.20	1000.9	1131.1	0.2349	1.6094	1.8443	5.0
10.0	193.21	0.016592	14404	14404	161.26	982.1	1143.3	0.2836	1.5043	1.7879	10.0
14.696	212.00	0.016719	12782	12782	180.17	970.3	1150.5	0.3121	1.4447	1.7568	14.696
15.0	213.03	0.016726	12627.4	12629	181.21	969.7	1150.9	0.3137	1.4415	1.7552	15.0
20.0	227.96	0.016834	10700	10707	196.27	960.1	1156.3	0.3358	1.3962	1.7320	20.0
30.0	250.34	0.017009	9059.7	9065.6	218.9	945.2	1164.1	0.3682	1.3313	1.6995	30.0
40.0	267.25	0.017151	8009.2	8015.1	236.1	933.6	1169.8	0.3921	1.2844	1.6765	40.0
50.0	281.02	0.017274	7299.7	7305.6	250.2	923.9	1174.1	0.4112	1.2474	1.6586	50.0
60.0	292.71	0.017383	6755.2	6761.1	262.2	915.4	1177.6	0.4273	1.2167	1.6440	60.0
70.0	302.93	0.017482	6317.5	6323.4	272.7	907.8	1180.6	0.4411	1.1905	1.6316	70.0
80.0	312.04	0.017573	5956.4	5962.3	282.1	900.9	1183.1	0.4534	1.1675	1.6208	80.0
90.0	320.28	0.017659	5647.9	5653.8	290.7	894.6	1185.3	0.4643	1.1470	1.6113	90.0
100.0	327.82	0.017740	5382.5	5388.4	298.5	888.6	1187.2	0.4743	1.1284	1.6027	100.0
110.0	334.79	0.01782	5155.7	5161.6	305.8	883.1	1188.9	0.4834	1.1115	1.5950	110.0
120.0	341.27	0.01789	4964.3	4970.2	312.6	877.8	1190.4	0.4919	1.0960	1.5879	120.0
130.0	347.33	0.01796	4799.2	4805.1	319.0	872.8	1191.7	0.4998	1.0815	1.5813	130.0
140.0	353.04	0.01803	4655.5	4661.4	325.0	868.0	1193.0	0.5071	1.0681	1.5752	140.0
150.0	358.43	0.01809	4528.9	4534.8	330.6	863.4	1194.1	0.5141	1.0554	1.5695	150.0
160.0	363.55	0.01815	4415.2	4421.1	336.1	859.0	1195.1	0.5206	1.0435	1.5641	160.0
170.0	368.42	0.01821	4311.3	4317.2	341.2	854.8	1196.0	0.5269	1.0322	1.5591	170.0
180.0	373.08	0.01827	4215.2	4221.1	346.2	850.7	1196.9	0.5328	1.0215	1.5543	180.0
190.0	377.53	0.01833	4125.9	4131.8	350.9	846.7	1197.6	0.5384	1.0113	1.5498	190.0
200.0	381.80	0.01839	4042.5	4048.4	355.5	842.8	1198.3	0.5438	1.0016	1.5454	200.0
210.0	385.91	0.01844	3973.7	3979.6	359.9	839.1	1199.0	0.5490	0.9923	1.5413	210.0
220.0	389.88	0.01850	3917.5	3923.4	364.2	835.4	1199.6	0.5540	0.9834	1.5374	220.0
230.0	393.70	0.01855	3871.9	3877.8	368.3	831.8	1200.1	0.5588	0.9748	1.5336	230.0
240.0	397.39	0.01860	3835.2	3841.1	372.3	828.4	1200.6	0.5634	0.9665	1.5299	240.0
250.0	400.97	0.01865	3805.8	3811.7	376.1	825.0	1201.1	0.5679	0.9585	1.5264	250.0
260.0	404.44	0.01870	3781.5	3788.0	379.9	821.6	1201.5	0.5722	0.9508	1.5230	260.0
270.0	407.80	0.01875	3761.2	3767.7	383.6	818.3	1201.9	0.5764	0.9433	1.5197	270.0
280.0	411.07	0.01880	3744.1	3750.6	387.1	815.1	1202.3	0.5805	0.9361	1.5166	280.0
290.0	414.25	0.01885	3729.9	3736.4	390.6	812.0	1202.6	0.5844	0.9291	1.5135	290.0
300.0	417.35	0.01889	3717.5	3723.9	394.0	808.9	1202.9	0.5882	0.9223	1.5105	300.0
350.0	431.73	0.01912	3653.4	3659.8	409.8	794.2	1204.0	0.6059	0.8909	1.4968	350.0
400.0	444.60	0.01934	3578.4	3584.8	424.2	780.4	1204.6	0.6217	0.8630	1.4847	400.0
450.0	456.28	0.01954	3502.8	3509.2	437.3	767.5	1204.8	0.6360	0.8378	1.4738	450.0
500.0	467.01	0.01975	3431.9	3438.3	449.5	755.1	1204.7	0.6490	0.8148	1.4639	500.0
550.0	476.94	0.01994	3367.5	3373.9	460.9	743.3	1204.3	0.6611	0.7936	1.4547	550.0
600.0	486.20	0.02013	3309.0	3315.4	471.7	732.0	1203.7	0.6723	0.7738	1.4461	600.0
650.0	494.89	0.02032	3254.8	3261.2	481.9	720.9	1202.8	0.6828	0.7552	1.4381	650.0
700.0	503.08	0.02050	3204.5	3210.9	491.6	710.2	1201.8	0.6928	0.7377	1.4304	700.0
750.0	510.84	0.02069	3157.8	3164.2	500.9	699.8	1200.7	0.7022	0.7210	1.4232	750.0
800.0	518.21	0.02087	3114.2	3120.6	509.8	689.6	1199.4	0.7111	0.7051	1.4163	800.0
850.0	525.24	0.02105	3072.5	3078.9	518.4	679.5	1198.0	0.7197	0.6899	1.4096	850.0
900.0	531.95	0.02123	3032.5	3038.9	526.7	669.7	1196.4	0.7279	0.6753	1.4032	900.0
950.0	538.39	0.02141	2994.0	3000.4	534.7	660.0	1194.7	0.7358	0.6612	1.3970	950.0
1000.0	544.58	0.02159	2957.0	2963.4	542.6	650.4	1192.9	0.7434	0.6476	1.3910	1000.0
1050.0	550.53	0.02177	2921.5	2927.8	550.1	640.9	1191.0	0.7507	0.6344	1.3851	1050.0
1100.0	556.28	0.02195	2887.5	2893.8	557.5	631.5	1189.1	0.7578	0.6216	1.3794	1100.0
1150.0	561.82	0.02214	2854.5	2860.8	564.8	622.2	1187.0	0.7647	0.6091	1.3738	1150.0
1200.0	567.19	0.02232	2822.5	2829.0	571.9	613.0	1184.8	0.7714	0.5969	1.3683	1200.0
1250.0	572.38	0.02250	2791.5	2798.0	578.8	603.8	1182.6	0.7780	0.5850	1.3630	1250.0
1300.0	577.42	0.02269	2761.5	2768.0	585.6	594.6	1180.2	0.7843	0.5733	1.3577	1300.0
1350.0	582.32	0.02288	2732.5	2739.0	592.3	585.4	1177.8	0.7906	0.5620	1.3525	1350.0
1400.0	587.07	0.02307	2704.5	2711.0	598.8	576.5	1175.3	0.7966	0.5507	1.3474	1400.0
1450.0	591.70	0.02327	2677.5	2684.0	605.3	567.4	1172.8	0.8026	0.5397	1.3423	1450.0
1500.0	596.20	0.02346	2651.5	2658.0	611.7	558.4	1170.1	0.8085	0.5288	1.3373	1500.0
1550.0	600.59	0.02366	2626.5	2633.0	618.0	549.4	1167.4	0.8142	0.5182	1.3324	1550.0
1600.0	604.87	0.02387	2602.5	2609.0	624.2	540.3	1164.5	0.8199	0.5076	1.3274	1600.0
1650.0	609.05	0.02407	2579.5	2586.0	630.4	531.3	1161.6	0.8254	0.4971	1.3225	1650.0
1700.0	613.13	0.02428	2557.5	2564.0	636.5	522.2	1158.6	0.8309	0.4867	1.3176	1700.0
1750.0	617.12	0.02450	2536.5	2543.0	642.5	513.1	1155.6	0.8363	0.4765	1.3128	1750.0
1800.0	621.02	0.02472	2516.5	2523.0	648.5	503.8	1152.3	0.8417	0.4662	1.3079	1800.0
1850.0	624.83	0.02495	2497.5	2504.0	654.5	494.6	1149.0	0.8470	0.4561	1.3030	1850.0
1900.0	628.56	0.02517	2479.5	2486.0	660.4	485.2	1145.6	0.8522	0.4459	1.2981	1900.0
1950.0	632.22	0.02541	2462.5	2469.0	666.3	475.8	1142.0	0.8574	0.4358	1.2931	1950.0
2000.0	635.80	0.02565	2446.5	2453.0	672.1	466.2	1138.3	0.8625	0.4256	1.2881	2000.0
2100.0	642.76	0.02615	2412.5	2419.0	683.8	446.7	1130.5	0.8727	0.4053	1.2780	2100.0
2200.0	649.45	0.02669	2379.5	2386.0	695.5	426.7	1122.2	0.8828	0.3848	1.2676	2200.0
2300.0	655.89	0.02727	2347.5	2354.0	707.2	406.0	1113.2	0.8929	0.3640	1.2569	2300.0
2400.0	662.11	0.02790	2316.5	2323.0	719.0	384.8	1103.7	0.9031	0.3430	1.2460	2400.0
2500.0	668.11	0.02859	2286.5	2294.0	731.7	361.6	1093.3	0.9139	0.3206	1.2345	2500.0
2600.0	673.91	0.02938	2257.5	2266.0	744.5	337.5	1082.0	0.9247	0.2977	1.2225	2600.0
2700.0	679.53	0.03029	2229.5	2239.0	757.3	312.3	1069.7	0.9356	0.2741	1.2097	2700.0
2800.0	684.96	0.03134	2202.5	2213.0	770.7	285.1	1055.8	0.9468	0.2491	1.1958	2800.0
2900.0	690.22	0.03262	2177.5	2189.0	785.1	254.7	1039.8	0.9588	0.2215	1.1803	2900.0
3000.0	695.33	0.03428	2154.5	2167.0	801.8	218.4	1020.3	0.9728	0.1891	1.1619	3000.0
3100.0	700.28	0.03681	2132.5	2147.0	824.0	159.3	993.3	0.9914	0.1460	1.1373	3100.0
3200.0	705.08	0.04472	2111.5	2128.0	875.5	56.1	931.6	1.0351	0.0482	1.0832	3200.0
3200.2*	705.47	0.05078	2100.0	2117.0	906.0	0.0	906.0	1.0612	0.0000	1.0612	3200.2*

*Critical pressure

13



Day 1**Radiation Protection**

13. The release rate of Ar-41 at a reactor stack is $10 \mu\text{Ci/s}$. The radionuclide emits a 1.27 MeV gamma ray. Atmospheric conditions are: wind speed, 4.0 m/s, stability condition B (at 1.0 km distance, $\sigma_y = 150 \text{ m}$; $\sigma_z = 150 \text{ m}$). The stack height is 100 m.
- Calculate the concentration of Ar-41 at the plume centerline, in $\mu\text{Ci/m}^3$, at a distance of 1.0 km from the stack.
 - Estimate the dose rate, in mrem/h, at that location, assuming that the concentration of Ar-41 in air is uniformly $X \mu\text{Ci/m}^3$.
 - Discuss the major factors that, under actual conditions, affect the accuracy of calculation (a).



Day 1**Radiation Protection**

14. A worker routinely ingests P-32 ($t_{1/2} = 14.3$ d, pure beta emitter, max. energy = 1.7 MeV). Assume that the radionuclide is uniformly distributed in the 70-kg worker. The physiological turnover rate of phosphorus compounds is 0.028 per day. The worker is limited to an annual dose of 1.0 rem.
- Calculate the effective half-life of P-32 in the body, in days.
 - Calculate the daily intake limit for P-32, in μCi , assuming that no other radiation exposure occurs.



DEC 12 1998

RESERVE DESK

GEORGIA INSTITUTE OF TECHNOLOGY

The George W. Woodruff School of Mechanical Engineering

Nuclear Engineering

Ph.D. Qualifying Exam

Fall Quarter, 1998

Day 2

Instructions

Your Code No.: _____

- 1. Complete 8* of the 11 questions.**
- 2. Use a separate page for each answer sheet (no front to back answers).**
- 3. Put **your code** on each of your answer sheets.**
- 4. The question number should be shown on each answer sheet.**
- 5. Staple your question sheet to your answer sheets and turn in.**

***Do NOT do more than 8 problems. If more than the requested number of problems are answered, then only the first 8 with the least scores will be counted towards the total score.**

Day 2

Kinetics and Depletion

1. Write the space- and time-dependent equations that govern the kinetics of a nuclear reactor in the one energy group diffusion theory, one delayed neutron group approximation. Derive the point kinetics approximation and give definitions for the parameters. Solve the point kinetics equations in the 'prompt-jump approximation' for an instantaneous insertion of negative reactivity into an initially critical reactor.

Day 2

Kinetics and Depletion

2. Write the equations that describe, at a point in a uranium-fueled nuclear reactor, the depletion of U-235, the buildup of Pu-239 and the buildup of fission products. Use a one energy group description. Define all terms. Write an equation for the 'breeding ratio'. Explain how the negative reactivity associated with the fuel depletion and fission product buildup may be compensated to maintain criticality.

Day 2

Diffusion Theory

3. Isotropic point sources each emitting S neutrons/sec are placed in an infinite moderator at the four corners of a square of side a . Compute the flux and current at the midpoint of any side of the square and at its center.

The following formula might help.

$$\phi = \frac{S}{4\pi D r} e^{-r/L}$$

Day 2**Transport Theory**

4. Consider the one-speed transport equation in a purely absorbing slab with a constant (flat) isotropic source:

$$\mu \frac{\partial \psi(z, \mu)}{\partial z} + \psi(z, \mu) = a, \quad 0 \leq z \leq 1$$

where,

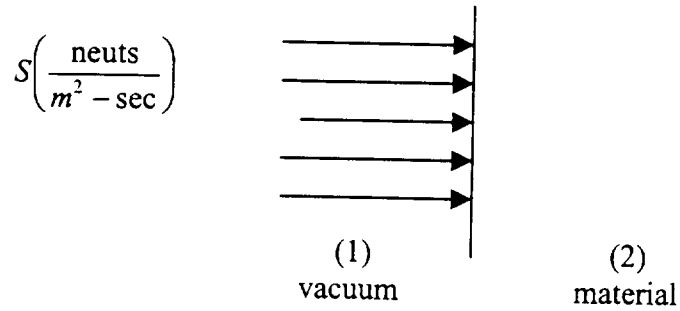
$$a = \text{constant}$$

Find the outgoing angular flux at $z = 1$ using vacuum boundary conditions.

Day 2

Multigroup Diffusion Theory

5. Consider a two group problem with a beam of fast neutrons striking a semi-infinite slab.



Assuming **no** fissions.

- Write down the appropriate two-group equations.
- Write down the appropriate boundary conditions for each group.
- Outline how you would solve the differential equations.

6. For a uniform infinite mixture of two materials,

- A light (small mass number) moderator denoted by "M",
- A heavy (large mass number) absorber denoted by "A",

the infinite medium spectrum equation, in the vicinity of a low-energy isolated narrow resonance in the absorber, is

$$\Sigma_t(E)\varphi(E) = \int_E^{E/\alpha_M} \frac{\Sigma_s^M(E')\varphi(E')}{(1-\alpha_M)E'} dE' + \int_E^{E/\alpha_A} \frac{\Sigma_s^A(E')\varphi(E')}{(1-\alpha_A)E'} dE',$$

$$\varphi(E) \approx \frac{1}{E} \text{ above the resonance.}$$

Use the NR and NRIM approximations in the appropriate integrals to obtain a useful approximation to $\varphi(E)$ within the resonance. Physically justify the approximations that you use in each integral.

Day 2**Transport Theory**

7. Derive the self-adjoint form of the transport equation:

$$\mu \frac{\partial \psi(z, \mu)}{\partial Z} + \psi = \frac{c}{2} \int_{-1}^1 d\mu' \psi(z, \mu') \quad (1)$$

Hint: Write the angular flux as the summation of even and odd components in μ :

$$\psi(z, \mu) = \psi^+(z, \mu) + \psi^-(z, \mu), \quad (2)$$

where

$$\psi^+ = \text{even in } \mu$$

$$\psi^- = \text{odd in } \mu$$

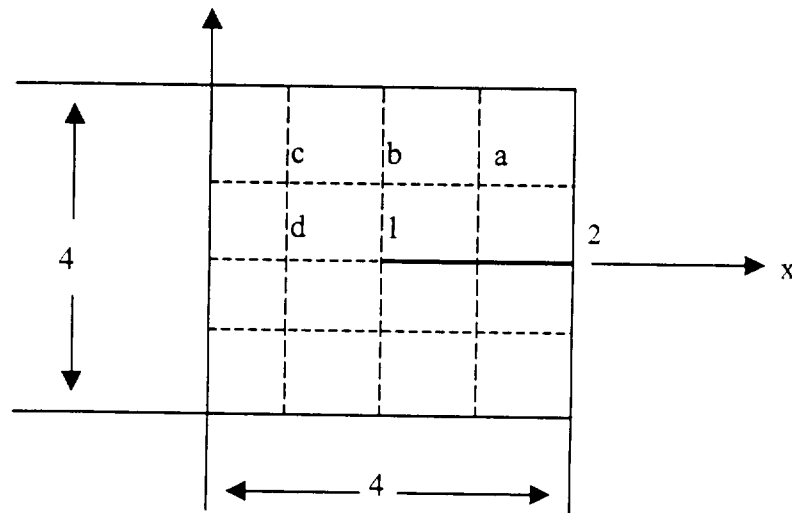
Day 2

Numerical Method

8. a. The indicated square region whose sides are length 4 is governed by the Helmholtz equation

$$\nabla^2 w + w = x$$

and has boundary conditions of $w = 1$ around the edge and along the line 1-2. Set up the finite difference equations approximating the equation using the indicated mesh size spacing of 1. Use the indicated notation for the variable at the mesh points and take advantage of symmetry around the x axis.

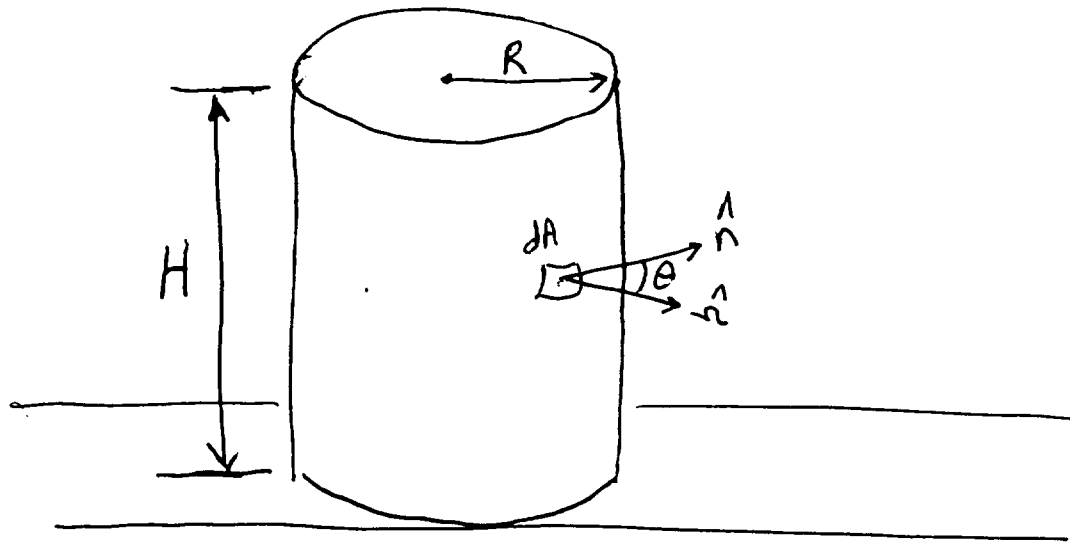


- b. Set up the Gauss-Seidel method of iteration for solving the resulting finite difference equations and go through two complete iteration cycles toward the solution.

Day 2

Monte Carlo Method

9. A cylindrical surface source which represents a dry storage cask for spent fuel is to be sampled. Gamma rays are emitted from the curved surface of the cylinder and the top surface. Recent results have shown that the gamma rays are emitted with the following angular probability distribution function, $p(\cos \theta) = 0.25 + 1.5 \cos \theta$. θ is the angle with respect to the surface normal at the point of emission. Assume that gamma-rays are only emitted in an outward direction from the surfaces of the cylinder, i.e. $0 \leq \theta \leq \pi/2$.
- a. Create an algorithm to uniformly sample the gamma ray source on the curved surface of the cylinder. Give the equations to randomly select the source location (X_s, Y_s, Z_s) .
 - b. Create a similar algorithm for uniformly selecting an (X_s, Y_s, Z_s) emission point on the top surface of the cylinder.
 - c. The emission angle (θ) of the gamma-ray can be selected from the $p(\cos \theta) = 0.25 + 1.5 \cos \theta$ distribution by using the alternate pdf technique. In this technique the pdf is split into two pdf's for sampling. How would these pdf's be created and how they would be sampled.



Day 2**Reactor Lab**

10. The multiplication, M , of a subcritical assembly may be defined as the ratio of the number of neutrons per unit time appearing in the assembly to the number per unit time that would appear because of the source alone:

$$M = \frac{\nu F + S}{S}$$

where

ν = average number of neutrons per fission

F = fission rate

S = external (nonfission) source rate.

In a subcritical multiplication experiment, S is a constant and M is measured in the steady state following a change in either the composition or the geometry. M is usually measured by a detector in or near the subcritical assembly.

- On what does the recorded multiplication depend on in addition to composition and geometry of the subcritical assembly.
- What is the relationship between M and the effective multiplication factor k ?
- The observed multiplication in such an experiment is calculated as

$$M_{obs} = \frac{C}{C_o}$$

where C_o is the count rate due to the source alone (no fission neutrons) and C is the count rate recorded by the detector in or near the assembly. What difficulties are anticipated in relating M_{obs} to the true multiplication?

Day 2

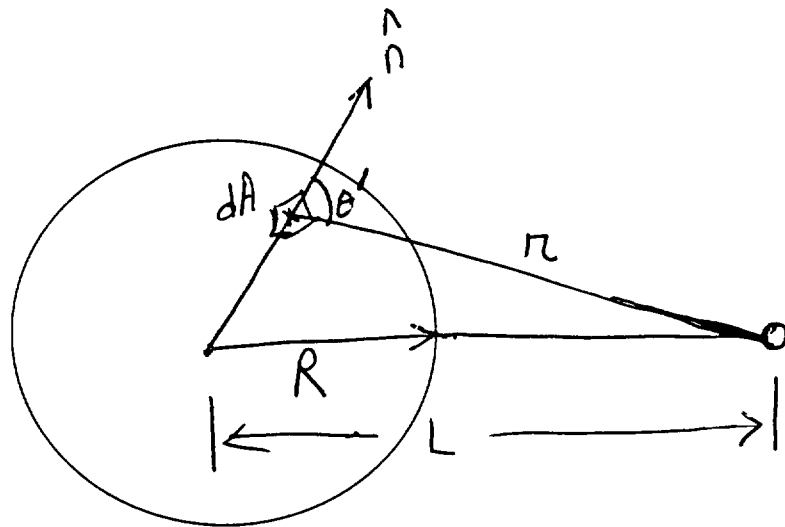
Shielding

11. The source on the surface of a sphere is cosine distributed, i.e. $S_a(\hat{r}) = A \cos \theta'$ neutrons/cm²-sr where A is a constant.

- a. What is the scalar flux on the surface of the sphere?
- b. Show that the scalar flux at a distance L from the center of the sphere is

$$\phi(L) = 2 \pi A \left[1 - \sqrt{1 - \left(\frac{R}{L}\right)^2} \right]$$

- c. What is the magnitude of the current at the distance L from the sphere?



RESERVE DESK

DEC 12 1998

GEORGIA INSTITUTE OF TECHNOLOGY

The George W. Woodruff School of Mechanical Engineering

Nuclear Engineering

Ph.D. Qualifying Exam

Fall Quarter, 1998

Day 3

Instructions

Your Code No.: _____

1. Complete 6* of the 10 questions Plus the Design Question.
2. Use a separate page for each answer sheet (no front to back answers).
3. Put **your code** on each of your answer sheets.
4. The question number should be shown on each answer sheet.
5. Staple your question sheet to your answer sheets and turn in.

*Do NOT do more than 6 problems plus the design question. If more than the requested number of problems are answered, then only the design problem plus the first 6 with the least scores will be counted towards the total score.

Please **print** your name here.

**The Exam Committee will get a copy of this exam and will not be notified
whose paper it is until it is graded.**

Day 3

Single-Phase Flow Convection

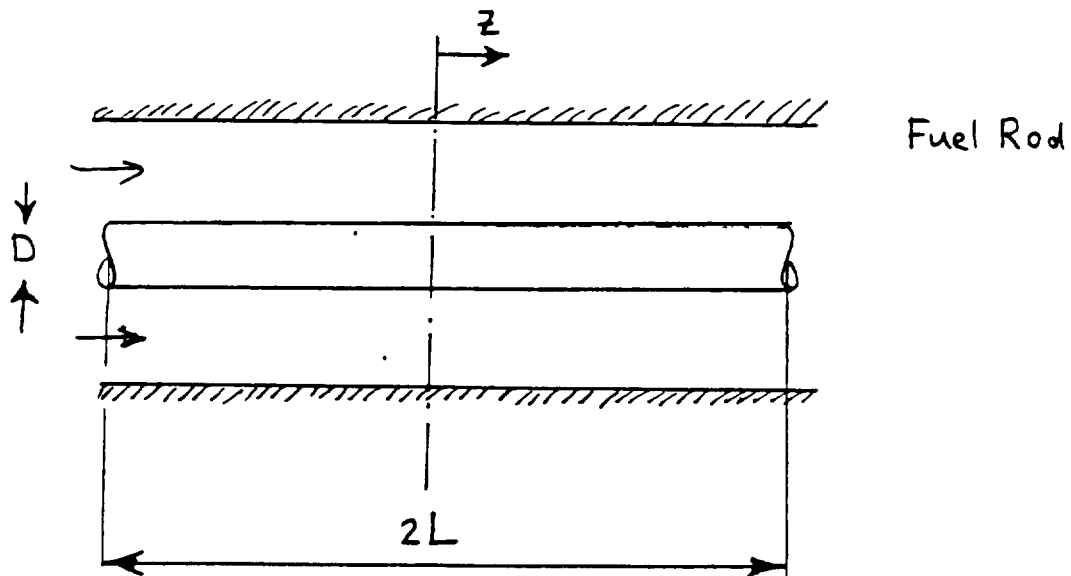
1. In the cylindrical fuel rod with length $2L$ and diameter D , volumetric heat is generated at the rate of

$$\dot{q} = \dot{q}_o \cos\left(\frac{\pi x}{L}\right)$$

The fuel rod is cooled by a coolant flowing at a mass flow rate \dot{m} , through the annular channel. The outer surface of the channel is well-insulated. The properties of the coolant can be assumed constant.

Obtain expressions for:

- mean coolant temperature, $T_m(x)$;
- fuel rod surface temperature, $T_s(x)$; and
- the location at which the fuel rod surface temperature is maximum.



Day 3**Boiling Heat Transfer**

2. Water flows upward in a round tube 1.0 cm in diameter. The pressure along the channel is assumed constant at 6 MPa, and at inlet the water is 50°C subcooled. The channel wall temperature is assumed to be constant at 295°C, and the water mass flux is $G = 10,000 \text{ kg/m}^2\text{s}$.

Find the axial locations where onset of nucleate boiling (ONB), onset of significant void (OSV), and fully-developed nucleate boiling occur.

For the water, assume:

$$\begin{aligned} T_{\text{sat}} &= 275.6 \text{ K} \\ h_{\text{fg}} &= 1.57 \times 10^6 \text{ J/kg} \\ C_{\text{PL}} &= 5000 \text{ J/kg K} \\ \rho &= 758 \text{ kg/m}^3 \\ \nu &= 0.13 \times 10^{-6} \text{ m}^2/\text{s} \\ k &= 0.577 \text{ W/mk} \end{aligned}$$

For convection heat transfer

$$\frac{hD}{k} = 0.023 \text{ Re}^{0.8} \text{ Pr}^{0.33}$$

- ONB correlation (Bergles and Rohsenow):

$$(T_w - T_{\text{sat}})_{\text{ONB}} = 0.556 \left[\frac{q''}{1082 p^{1.156}} \right]^n$$

$$n = 0.463 P^{0.0234}$$

P: bar

q'' : W/m^2

- Saha-Zuber correlation for OSV

$$(h_f - h_L)_{\text{OSV}} = 0.002 \frac{q'' D C_{\text{PL}}}{k_L} \text{ for } \text{Re Pr} < 7 \times 10^4$$

$$(h_f - h_L)_{\text{OSV}} = 154 \frac{q''}{G} \text{ for } \text{Re Pr} > 7 \times 10^4$$

Day 3

Heat Conduction

3. Consider two conditions for heat transfer in a BWR fuel pin: (1) initial uncracked pellets with no relocation, and (2) cracked and relocated fuel.
- a. For each condition, find the peak and volume-averaged fuel material temperature, and peak clad temperature.

Geometry and Material Information:

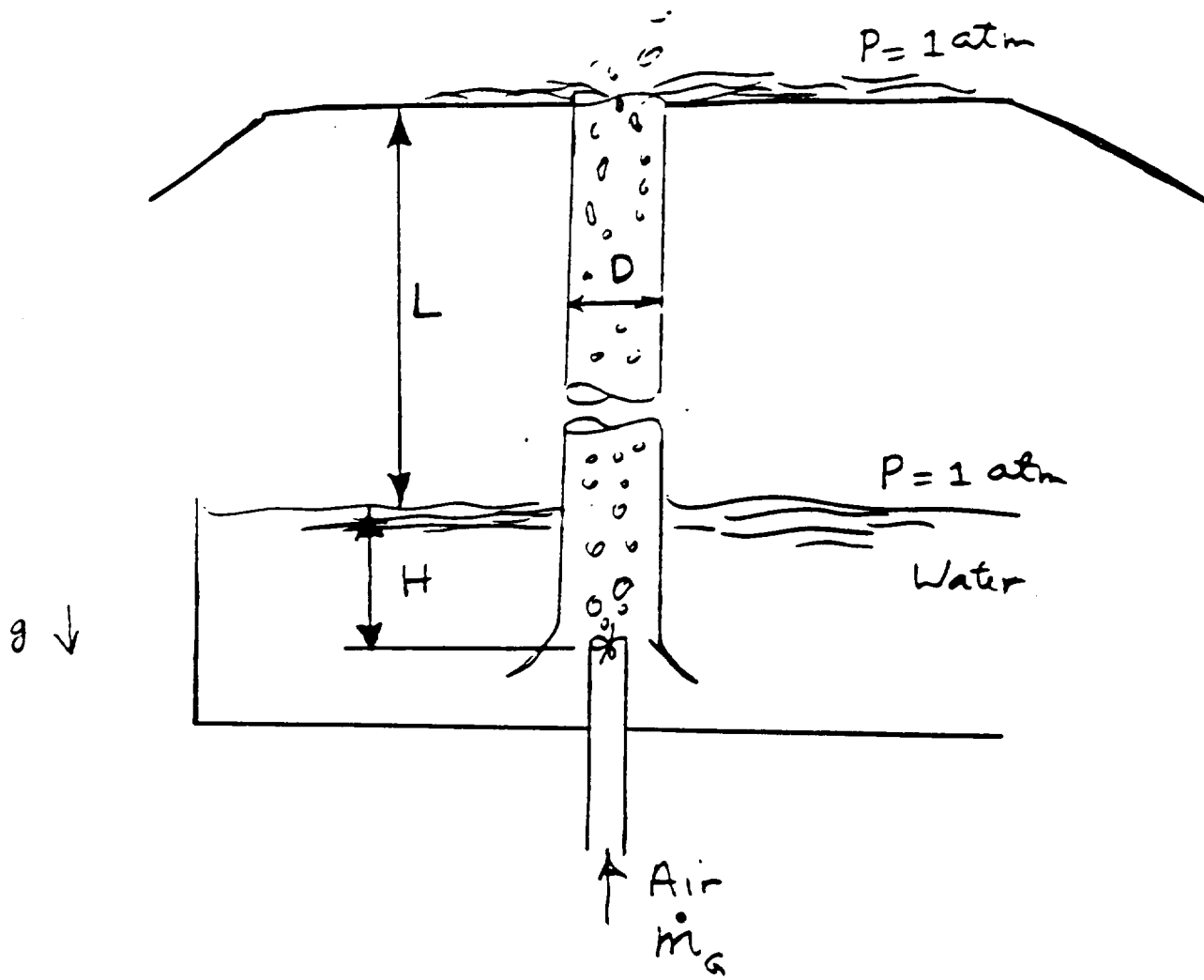
- Clad outside diameter = 12.50 mm
- Clad thickness = 0.85 mm
- Fuel/clad gap thickness = 0.15 mm
- Clad thermal conductivity = 17 W/m^{°K}
- Initial gap conductance = 4.0 kW/m^{2°K}
- Gap conductance after fuel relocation = 31 kW/m^{2°K}
- Uncracked fuel material conductivity = 2.7 W/m^{°K}
- Cracked fuel material conductivity = 2.3 W/m^{°K}
- Linear heat rate = 40 kW/m
- Clad outside surface temperature = 290°C

Day 3

Two-Phase Flow

4. Air is supplied at a constant mass flow rate of \dot{m}_G into the air lift pump shown in the figure. The pressure drops associated with channel entrance and exit are negligible. The vertical channel is long, such that entrance effects can be neglected. Water and air are both assumed to be incompressible.
- Derive an equation for the liquid mass flow rate, assuming the two phase flow in the channel is homogeneous.
 - Show how the equation derived in part (a) can be improved using the draft flux model. Assume C_0 and V_{gj} are known constants.

For both cases, use the turbulent homogeneous mixture flow assumption for frictional pressure drop, assuming a constant friction factor, f_L .



Day 3**Two-Phase Flow**

5. A 10-ft. high boiling-water channel operates at an average pressure of 1000 psia, 34.6°F inlet subcooling, 10 ft/sec inlet velocity, and 10% exit quality. The channel hydraulic diameter is 0.5 inches. The voids in the upper part of the channel cause neutron flux depression there, so that the axial flux distribution is represented by:

$$\phi = C e^{-\pi z/H} \sin \frac{\pi z}{H}$$

where C is a constant, $z = 0$ indicates the channel entrance, and H is the channel height.

- a. Determine the non-boiling and boiling heights. $\left[\int e^{ax} \sin x \, dx = \frac{e^{ax}}{a^2 + 1} (a \sin x - \cos x) \right]$
- b. Determine the two-phase friction pressure drop in the boiling height. [Ignore dependence of the average two-phase friction multiplier on the heat flux profile; for saturated water at 1000 psia: $\mu_f = 0.233 \text{ lb}_m/\text{ft hr.}$]

[Steam tables are attached (2 pages).]

CONVECTIVE BOILING AND CONDENSATION

have been published by Thom.¹³ These revised values were derived using an extensive set of experimental data for steam-water pressure drops obtained at Cambridge, England, on heated and unheated horizontal and vertical tubes. The alternative values of these quantities as suggested by Thom are given in Table 2.3.

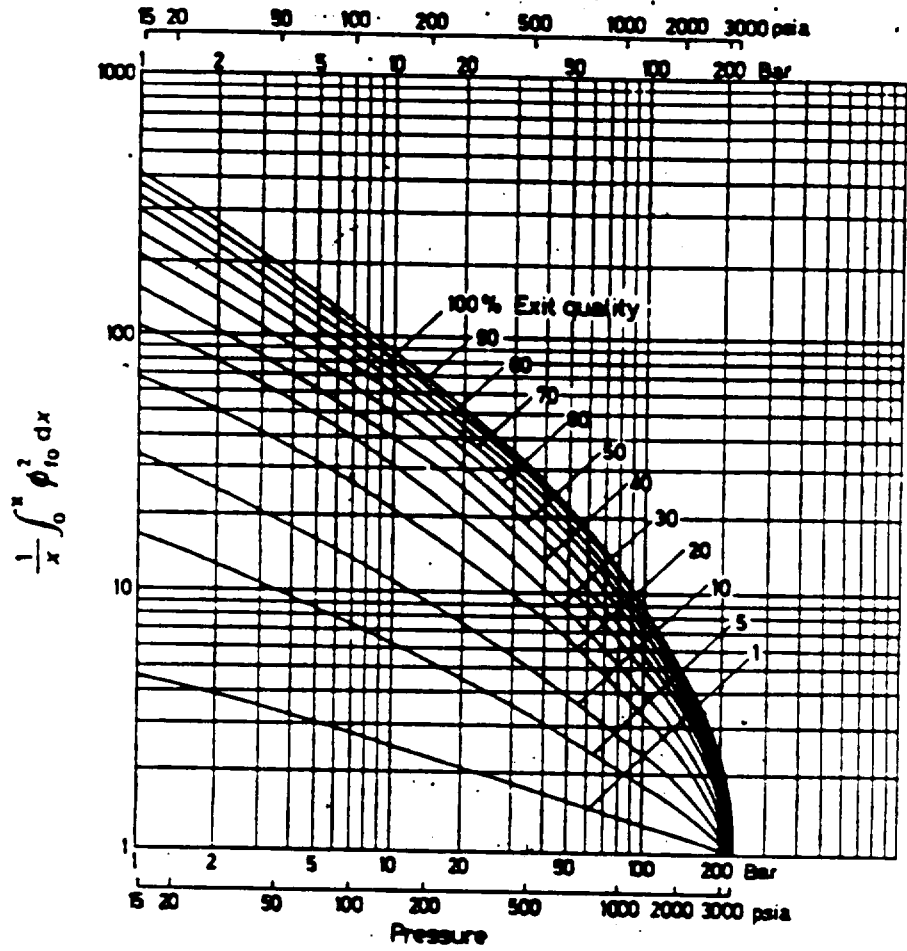


Fig. 2.5. $\frac{1}{x} \int_0^x \phi_{10}^2 dx$ as a Function of Quality and Absolute Pressure Steam-Water (Martinelli-Nelson)

2.4.5 The Application of the Separated Flow Model to Experimental Observations

The Lockhart-Martinelli-Nelson model has been used extensively for the correlation of experimental pressure gradients and void fraction measurements for both single and two-component gas-liquid flow. Generally, it is found that the separated flow model is capable of more accurate predictions than the homogeneous model.

Two general observations can be made concerning the application of the Lockhart-Martinelli correlation.

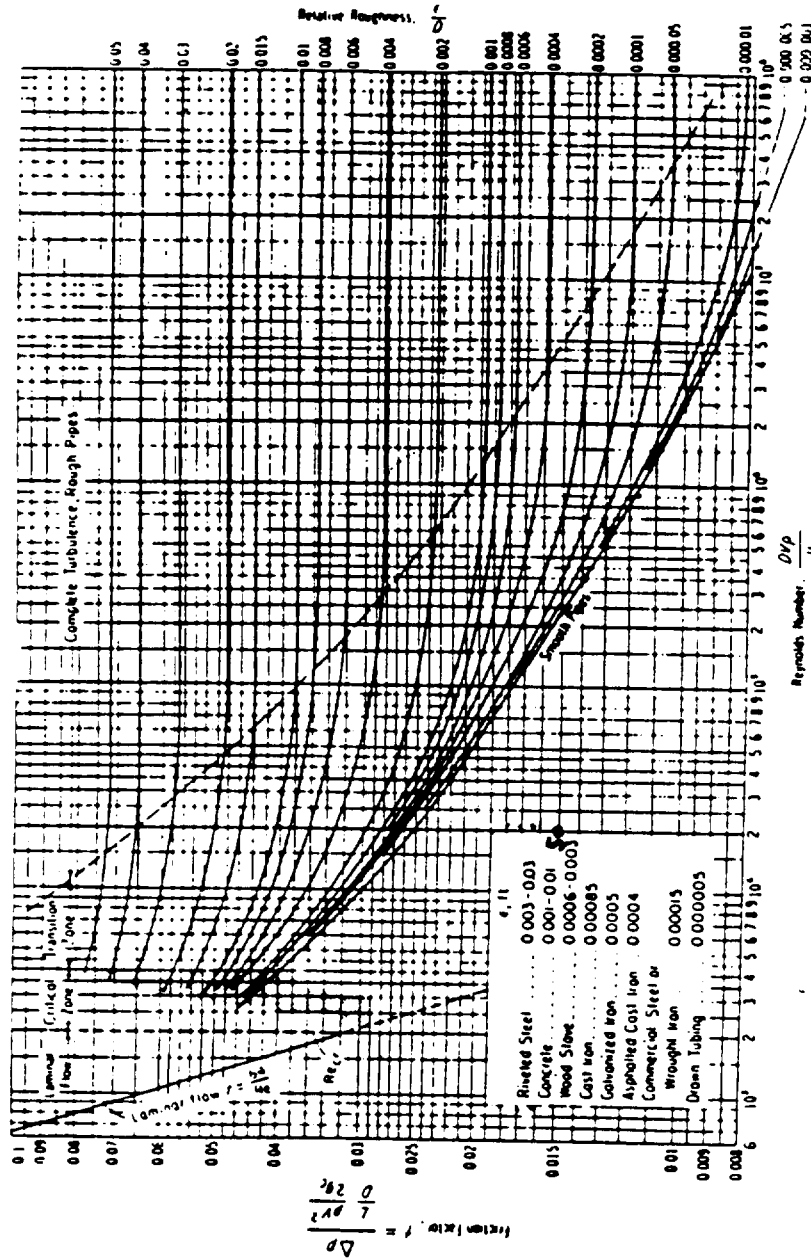


FIG F-1

appendix
So

Day 3

Materials

6. Sketch a Phase Diagram (also known as Equilibrium Diagram) for two materials (for example A and B) that show a eutectic but no solid solubility. Sketch the cooling curve for the eutectic composition. Also sketch the microstructure of a material having the eutectic composition after cooling to below the eutectic temperature. Describe what could happen if a piece of material A is placed in contact with a piece of Material B for a long time at high temperature as could occur in the core of a reactor or in an isotopic heat source. Assume the temperature at the point of contact is above the eutectic temperature.

Day 3

Materials

7. Describe in detail the changes that occur in mechanical properties and microstructure when a metal clad oxide nuclear fuel is irradiated to high burn-up at high power. Give your answer for both the cladding and oxide.

Day 3

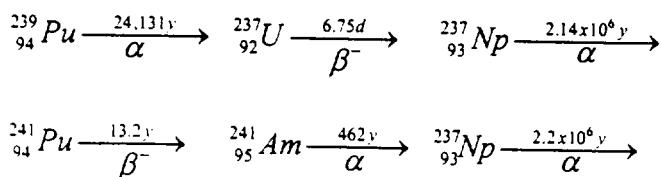
Fuel Cycle

8. It is proposed that ^{10}B be concentrated by the gaseous diffusion process applied to $^{10}\text{BF}_3$ and $^{11}\text{BF}_3$. The plant is to be designed as an ideal cascade and is to separate feed containing 19% ^{10}B into product containing 90% and tails containing 8%. The stage-separation factor is 1.0074. How many stages are needed in the stripping section? In the enriching section?

Day 3

Waste Management

9. Ten grams of PuF₆ are to be stored in a vault. The Pu is 25% ²⁴¹Pu and 75% ²⁴²Pu. Neutrons are emitted due to the (α,n) reaction with fluorine. The decay data for the plutonium isotopes is given below.
- Estimate the number of neutrons emitted initially by this source.
 - In 25 years, will more or fewer neutrons be emitted?
 - Elaborate on any shortcomings of your neutron emission estimates.



Isotope	Alpha Energy (MeV)
²³⁹ Pu	5.14 MeV
²⁴¹ Pu	---
²⁴¹ Am	5.496
²³⁷ Np	4.78

Table 1. Experimental (α,n) thick target element yields as a function of initial α energy, n/10⁶ α

Element	Initial α energy, MeV					
	4.0	4.5	5.0	5.5	6.0	6.5
Li	0.002	0.028	0.629	2.150	4.873	10.41
Be	19.88	33.27	49.43	71.81	99.16	126.2
B	6.238	10.63	15.64	20.59	25.35	29.85
C	0.0433	0.0497	0.0647	0.1116	0.1748	0.2555
O	0.0169	0.0312	0.0493	0.0722	0.1001	0.1324
O	0.014	0.028	0.045	0.0675	0.0904	0.120
F	0.879	2.159	4.394	7.746	12.26	17.95
Na	-	-	-	1.5	-	-
Mg	0.77	0.263	0.644	1.262	2.141	3.250
Al	0.0169	0.0802	0.2643	0.6967	1.438	2.780
Si	-	0.016	0.052	0.114	0.231	0.385
Fe	-	-	0.0002	0.0003	0.0042	0.0207

Day 3**Nuclear Design**

10. You are working for a company that locates and assays subsurface deposits of uranium. Your company is reasonably assured it has located a potentially profitable deposit of uranium. They want to drill boreholes and perform uranium well logging measurements. They want you to design an instrument to detect the presence of uranium and quantify its concentration and distribution in the ore deposit. This "tool" will be lowered into the boreholes.

Design such an instrument (obviously you cannot be overly quantitative). Some potentially helpful data is attached.

- Be sure to enumerate the possible active and passive nuclear techniques that can be used.
- Select one of the possibilities and elaborate on the technique and how you would implement it.

Additional Data:

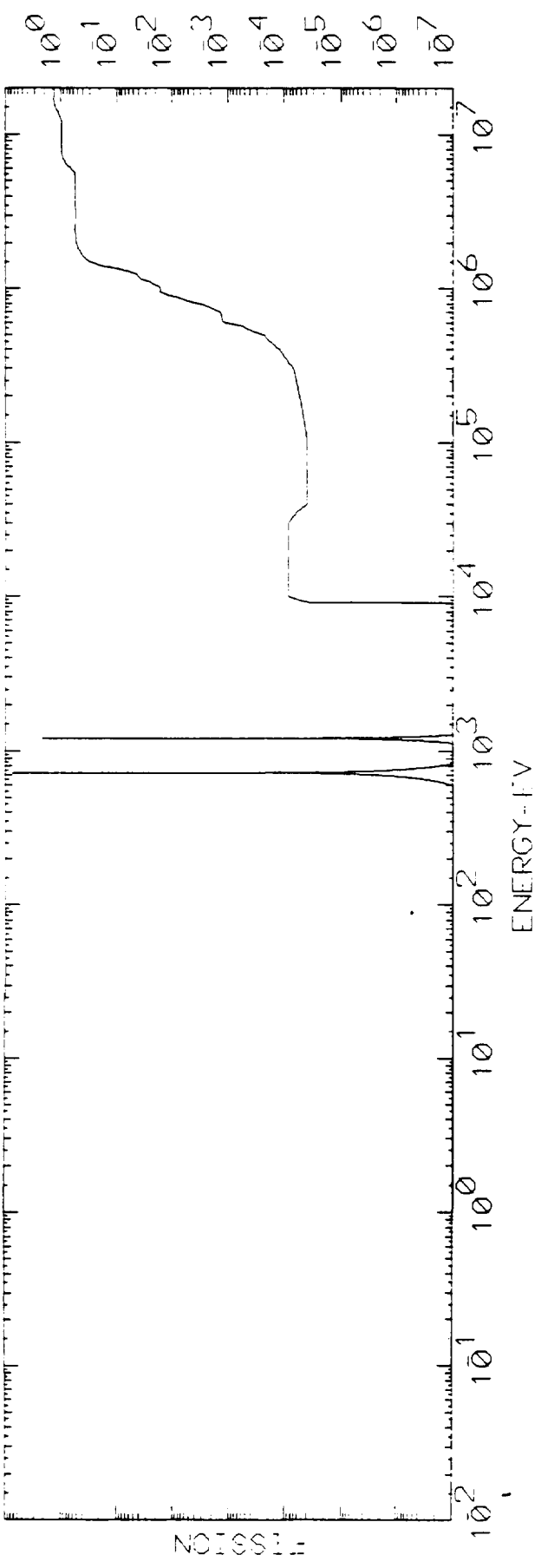


$${}^{238}\text{U}: \sigma_{th}^{(n, \gamma)} = 2.76$$

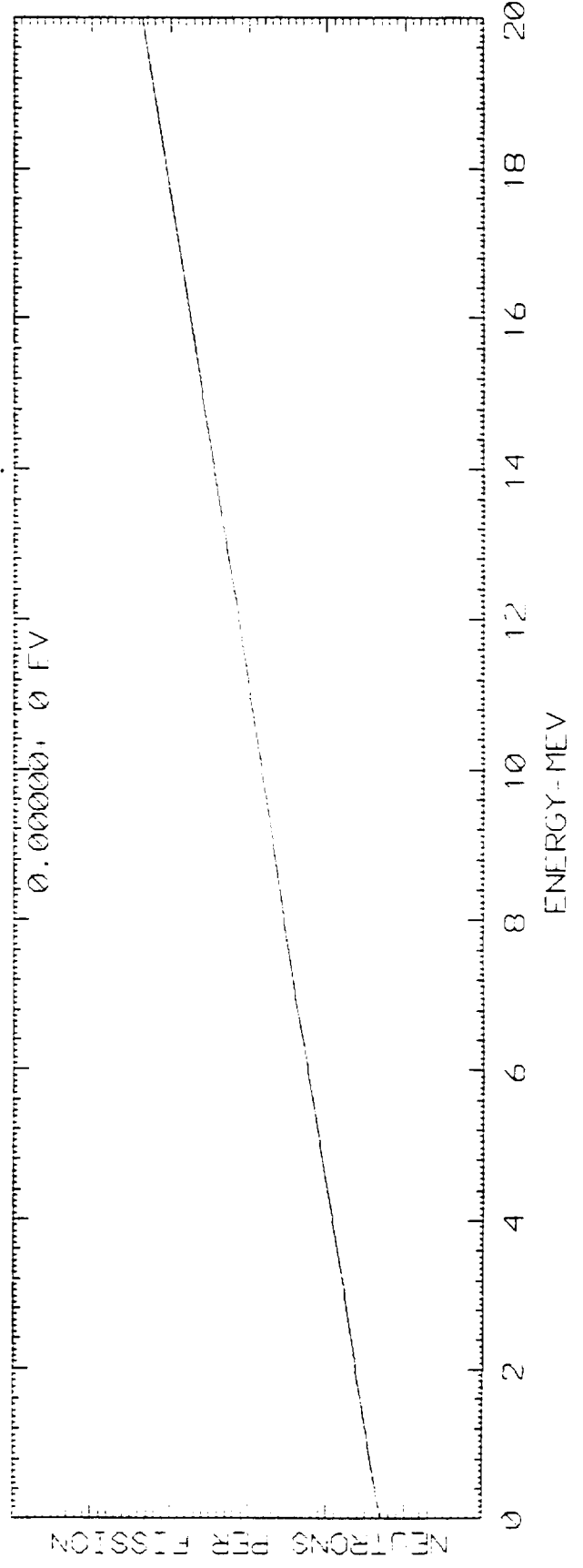
$$RI^{(n, \gamma)} = 2806$$

(4 pages attached)

URANIUM-238 ENDF/B MAT NO. 1262



CROSS SECTION-BARNS



NEUTRONS PER FISSION

URANIUM-235

ENDF/B MAT NO. 1261

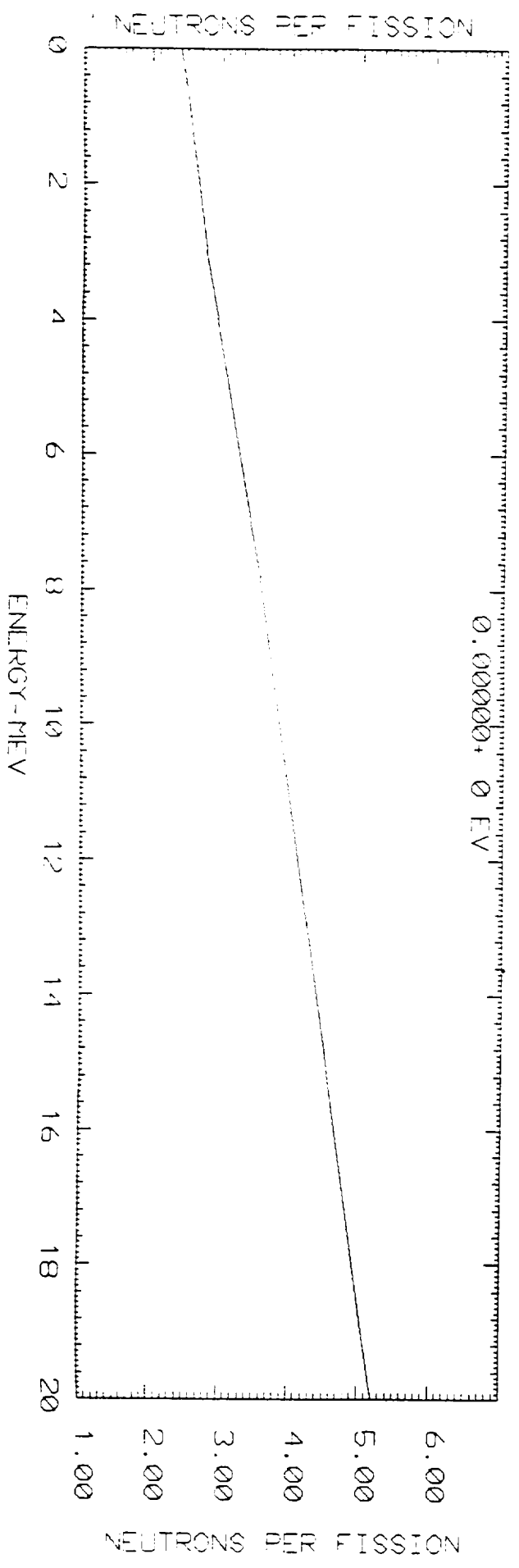
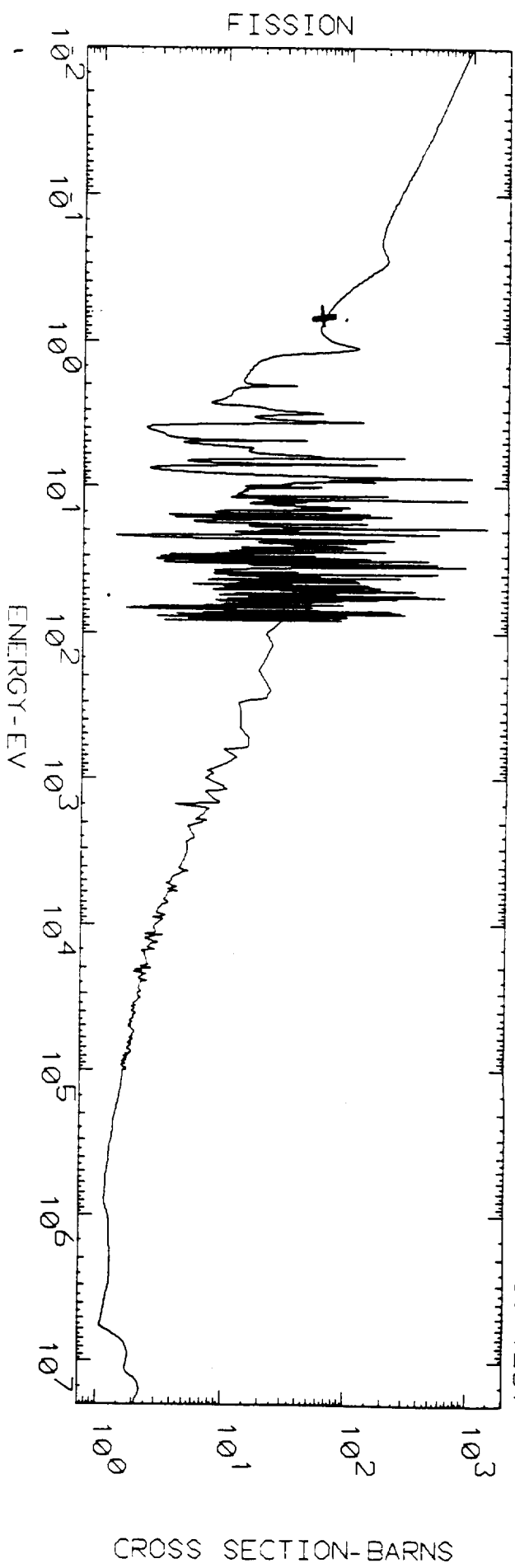


TABLE 4.4. Actinium Series ($4n + 3$)

Nuclide	Half-life	Energy, MeV		
		Alpha ^a	Beta	Gamma, photons/ trans. ^b
²³⁵ ₉₂ U	7.13 × 10 ⁸ years	4.39		0.18 (0.7)
²³¹ ₉₀ Th (UY)	25.64 h		0.094, 0.302, 0.216	0.022 (0.7) 0.0085 (0.4) 0.061 (0.16)
²³¹ ₉₁ Pa	3.43 × 10 ⁴ years	5.049		0.33 (0.05) 0.027 (0.05) 0.012 (0.01)
²²⁷ ₈₉ Ac	21.8 years	4.94 (1.2%) ^a	0.0455 (98.8%) ^c	
²²⁷ ₉₀ Th (RdAc)	18.4 days	6.03		0.24 (0.2) 0.05 (0.15)
²²³ ₈₇ Fr (AcK)	21 min		1.15	0.05 (0.40) 0.08 (0.24)
²²³ ₈₈ Ra (AcX)	11.68 days	5.750		0.270 (0.10) 0.155 (0.055)
²¹⁹ ₈₆ Em (An)	3.92 s	6.824		0.267 (0.086) 0.392 (0.048)
²¹⁵ ₈₄ Po (AcA)	1.83 × 10 ⁻³ s	7.635		
²¹¹ ₈₂ Pb (AcB)	36.1 min		1.14, 0.5	Complex spectrum, 0.065 to 0.829 MeV
²¹¹ ₈₃ Bi (AcC)	2.16 min	6.619 (99.68%) ^c	Energy not known (0.32%) ^c	0.35 (0.14) 0.88 (0.005) 0.56 (0.005)
²¹¹ ₈₄ Po (AcC')	0.52 s	7.434		
²⁰⁷ ₈₁ Tl (AcC'')	4.78 min		1.47	0.87 (0.005)
²⁰⁷ ₈₂ Pb	Stable			

^aOnly the highest-energy alpha is given. Complete information on alpha energies may be obtained from Sullivan's *Tri-linear Chart of Nuclides*. Government Printing Office, Washington, D.C., 1957.

^bOnly the most prominent gamma photons are listed. For the complete gamma-ray information, consult T. P. KOHMAN: Natural radioactivity, in H. Blatz (ed.): *Radiation Hygiene Handbook*. McGraw-Hill, New York, 1959, pp. 6-13. With permission.

^cIndicates branching. The percentage enclosed in the parentheses gives the proportional decay by the indicated mode.

TABLE 4.3. Uranium Series (47 + 2)

Nuclide	Half-life	Energy, MeV		
		Alpha ^a	Beta	Gamma, photons/ trans. ^b
²³⁸ ₉₂ U	4.51 × 10 ⁹ years	4.18		
²³⁴ ₉₀ Th (UX ₁)	24.10 days		0.193, 0.103	0.092 (0.04) 0.063 (0.03)
^{234m} ₉₁ Pa (UX ₂)	1.175 min		2.31	1.0 (0.015) 0.76 (0.0063), I.T.
²³⁴ ₉₁ Pa (UZ)	6.66 h		0.5	Many weak
²³⁴ ₉₂ U (UII)	2.48 × 10 ⁵ years	4.763		
²³⁰ ₉₀ Th (I ₀)	8.0 × 10 ⁴ years	4.685		0.068 (0.0059)
²²⁶ ₈₈ Ra	1,622 years	4.777		
²²² ₈₆ Rn (Rn)	3.825 days	5.486		0.51 (very weak)
²¹⁸ ₈₄ Po (RaA)	3.05 min	5.998	Energy not known (0.022%) ^c	0.186 (0.030)
²¹⁸ ₈₅ At (RaA')	2 s	6.63	Energy not known (0.1%) ^c	
²¹⁸ ₈₆ Rn (RaA'')	0.019 s	7.127		
²¹⁴ ₈₂ Pb (RaB)	26.8 min		0.65	0.352 (0.036) 0.295 (0.020) 0.242 (0.07)
²¹⁴ ₈₃ Bi (RaC)	19.7 min	5.505 (0.04%) ^c	1.65, 3.7 (99.96%) ^c	0.609 (0.295) 1.12 (0.131)
²¹⁴ ₈₄ Po (RaC')	1.64 × 10 ⁻⁴ s	7.680		
²¹⁰ ₈₁ Tl (RaC'')	1.32 min		1.96	2.36 (1) 0.783 (1) 0.297 (1)
²¹⁰ ₈₂ Pb (RaD)	19.4 years		0.017	0.0467 (0.045)
²¹⁰ ₈₃ Bi (RaE)	5.00 days		1.17	
²¹⁰ ₈₄ Po (RaF)	138.40 days	5.298		0.802 (0.000012)
²⁰⁶ ₈₂ Pb (RaG)	Stable			

^aOnly the highest-energy alpha is given. Complete information on alpha energies may be obtained from Sullivan's *Tri-linear Chart of Nuclides*, Government Printing Office, Washington, D.C., 1957.

^bOnly the most prominent gamma photons are listed. For the complete gamma-ray information, consult T. P. KOHMAN: Natural radioactivity, in H. Blatz (ed.): *Radiation Hygiene Handbook*, McGraw-Hill, New York, 1959, pp. 6-13. With permission.

^cIndicates branching. The percentage enclosed in the parentheses gives the proportional decay by the indicated mode.

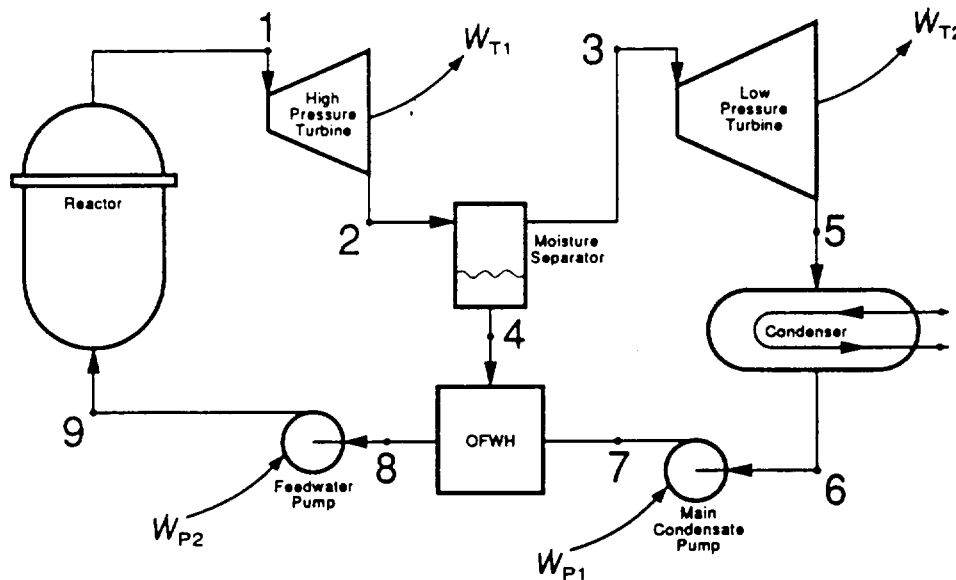
Day 3

Steam Cycles

11. The simplified BWR steam cycle shown in the figure uses one-stage moisture separation. The steam flow rate at the high pressure turbine inlet is $1.0 \times 10^6 \text{ lb}_m/\text{hr}$. The conditions in the table may be assumed. All turbines and pumps may be assumed to be ideal.

Point	Pressure (psia)	Condition
1	1000	Saturated vapor
2	200	
3	200	Saturated vapor
4	200	Saturated liquid
5	1	
6	1	Saturated liquid
7	200	
8	200	
9	1000	

- Sketch the T-S diagram for the cycle showing all points indicated in the table.
- Determine the power output for both the high pressure and low pressure turbines. [Steam tables and Mollier chart are attached (16 pages).]



Steam Cycles & Two-Phase Flow

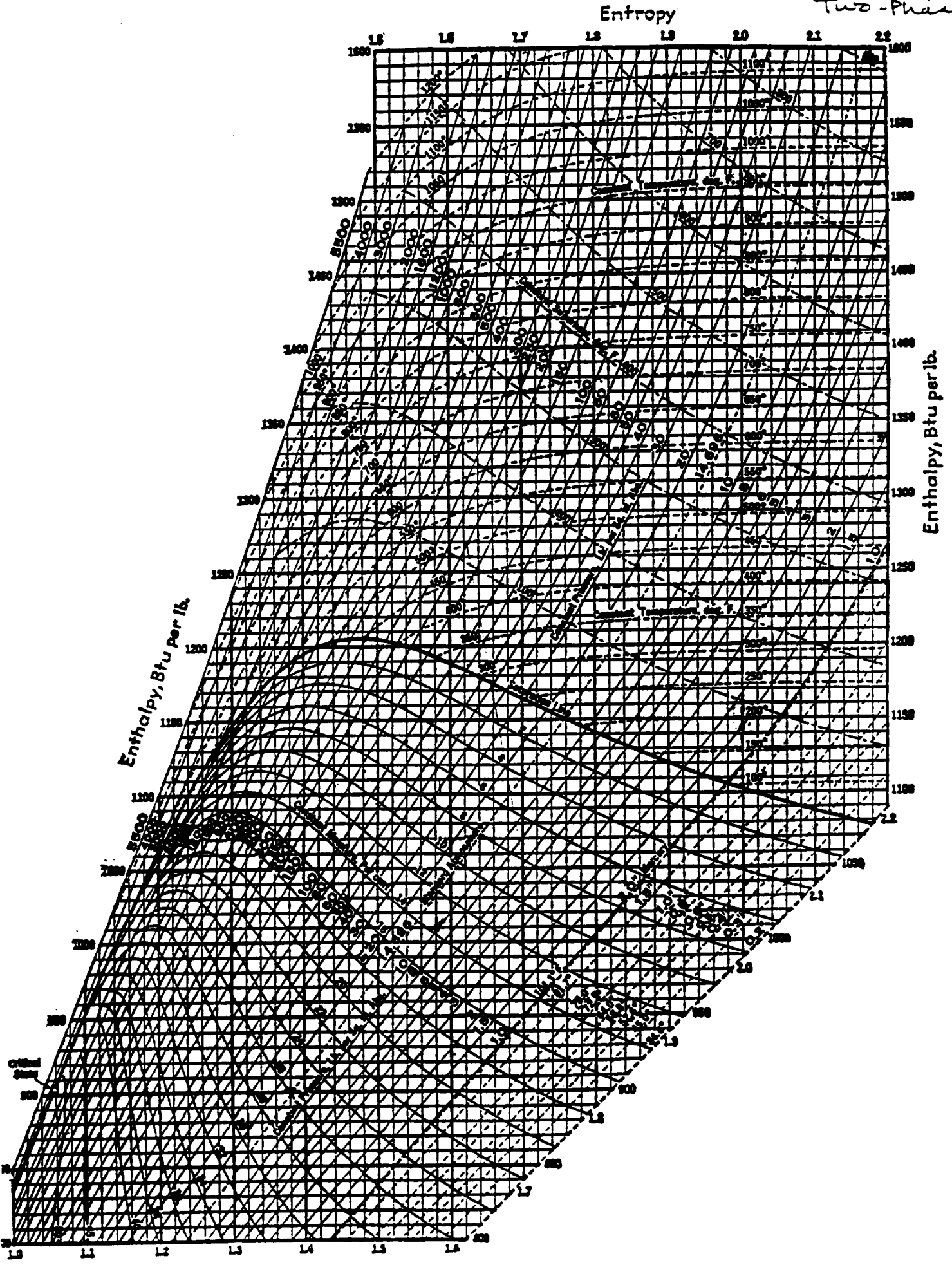


Table 1. Saturated Steam: Temperature Table

Temp Fahr t	Abs Press. Lb per Sq In. p	Specific volume			Enthalpy			Entropy			Temp Fahr t
		Sat. Liquid v _f	Evap v _{fg}	Sat. Vapor v _g	Sat. Liquid h _f	Evap h _{fg}	Sat. Vapor h _g	Sat. Liquid s _f	Evap s _{fg}	Sat. Vapor s _g	
32.0	0.08859	0.016022	3304.7	3304.7	-3.0179	1075.5	1075.5	0.0000	2.1873	2.1873	32.0
34.0	0.09600	0.016021	3061.9	3061.9	-3.396	1074.4	1076.4	0.0041	2.1762	2.1802	34.0
36.0	0.10395	0.016020	2839.0	2839.0	-3.808	1073.2	1077.2	0.0081	2.1651	2.1732	36.0
38.0	0.11249	0.016019	2634.1	2634.2	-4.018	1072.1	1078.1	0.0122	2.1541	2.1663	38.0
40.0	0.12163	0.016019	2445.8	2445.8	-4.3027	1071.0	1079.0	0.0162	2.1432	2.1594	40.0
42.0	0.13143	0.016019	2272.4	2272.4	-4.5935	1069.8	1079.9	0.0202	2.1325	2.1527	42.0
44.0	0.14192	0.016019	2112.8	2112.8	-4.9041	1068.7	1080.7	0.0242	2.1217	2.1459	44.0
46.0	0.15314	0.016020	1965.7	1965.7	-5.047	1067.6	1081.6	0.0282	2.1111	2.1393	46.0
48.0	0.16514	0.016021	1830.0	1830.0	-5.051	1066.4	1082.5	0.0321	2.1006	2.1327	48.0
50.0	0.17796	0.016023	1704.8	1704.8	-5.054	1065.3	1083.4	0.0361	2.0901	2.1262	50.0
52.0	0.19165	0.016024	1589.2	1589.2	-5.057	1064.2	1084.2	0.0400	2.0798	2.1197	52.0
54.0	0.20625	0.016026	1482.4	1482.4	-5.058	1063.1	1085.1	0.0439	2.0695	2.1134	54.0
56.0	0.22183	0.016028	1383.6	1383.6	-5.059	1061.9	1086.0	0.0478	2.0593	2.1070	56.0
58.0	0.23843	0.016031	1292.2	1292.2	-5.060	1060.8	1086.9	0.0516	2.0491	2.1008	58.0
60.0	0.25611	0.016033	1207.6	1207.6	-5.060	1059.7	1087.7	0.0555	2.0391	2.0946	60.0
62.0	0.27494	0.016036	1129.2	1129.2	-5.059	1058.5	1088.6	0.0593	2.0291	2.0885	62.0
64.0	0.29497	0.016039	1056.5	1056.5	-5.058	1057.4	1089.5	0.0632	2.0192	2.0824	64.0
66.0	0.31626	0.016043	989.0	989.1	-5.056	1056.3	1090.4	0.0670	2.0094	2.0764	66.0
68.0	0.33889	0.016046	926.5	926.5	-5.054	1055.2	1091.2	0.0708	1.9996	2.0704	68.0
70.0	0.36292	0.016050	868.3	868.4	-5.052	1054.0	1092.1	0.0745	1.9900	2.0645	70.0
72.0	0.38844	0.016054	814.3	814.3	-5.049	1052.9	1093.0	0.0783	1.9804	2.0587	72.0
74.0	0.41550	0.016058	764.1	764.1	-5.046	1051.8	1093.8	0.0821	1.9708	2.0529	74.0
76.0	0.44420	0.016063	717.4	717.4	-5.043	1050.7	1094.7	0.0858	1.9614	2.0472	76.0
78.0	0.47461	0.016067	673.8	673.9	-5.040	1049.5	1095.6	0.0895	1.9520	2.0415	78.0
80.0	0.50683	0.016072	633.3	633.3	-5.037	1048.4	1096.4	0.0932	1.9426	2.0359	80.0
82.0	0.54093	0.016077	595.5	595.5	-5.033	1047.3	1097.3	0.0969	1.9334	2.0303	82.0
84.0	0.57702	0.016082	560.3	560.3	-5.029	1046.1	1098.2	0.1006	1.9242	2.0248	84.0
86.0	0.61518	0.016087	527.5	527.5	-5.025	1045.0	1099.0	0.1043	1.9151	2.0193	86.0
88.0	0.65551	0.016093	496.8	496.8	-5.022	1043.9	1099.9	0.1079	1.9060	2.0139	88.0
90.0	0.69813	0.016099	468.1	468.1	-5.018	1042.7	1100.8	0.1115	1.8970	2.0086	90.0
92.0	0.74313	0.016105	441.3	441.3	-5.014	1041.6	1101.6	0.1152	1.8881	2.0033	92.0
94.0	0.79062	0.016111	416.3	416.3	-5.010	1040.5	1102.5	0.1188	1.8792	1.9980	94.0
96.0	0.84072	0.016117	392.8	392.9	-5.006	1039.3	1103.3	0.1224	1.8704	1.9928	96.0
98.0	0.89356	0.016123	370.9	370.9	-5.003	1038.2	1104.2	0.1260	1.8617	1.9876	98.0
100.0	0.94924	0.016130	350.4	350.4	-5.000	1037.1	1105.1	0.1295	1.8530	1.9825	100.0
102.0	1.00789	0.016137	331.1	331.1	-5.000	1035.9	1105.9	0.1331	1.8444	1.9775	102.0
104.0	1.06965	0.016144	313.1	313.1	-5.000	1034.8	1106.8	0.1366	1.8358	1.9725	104.0
106.0	1.1347	0.016151	296.16	296.18	-5.000	1033.6	1107.6	0.1402	1.8273	1.9675	106.0
108.0	1.2030	0.016158	280.28	280.30	-5.000	1032.5	1108.5	0.1437	1.8188	1.9626	108.0
110.0	1.2750	0.016165	265.37	265.39	-5.000	1031.4	1109.3	0.1472	1.8105	1.9577	110.0
112.0	1.3505	0.016173	251.37	251.38	-5.000	1030.2	1110.2	0.1507	1.8021	1.9528	112.0
114.0	1.4299	0.016180	238.21	238.22	-5.000	1029.1	1111.0	0.1542	1.7938	1.9480	114.0
116.0	1.5133	0.016188	225.84	225.85	-5.000	1027.9	1111.9	0.1577	1.7856	1.9433	116.0
118.0	1.6009	0.016196	214.20	214.21	-5.000	1026.8	1112.7	0.1611	1.7774	1.9386	118.0
120.0	1.6927	0.016204	203.25	203.26	-5.000	1025.6	1113.6	0.1646	1.7693	1.9339	120.0
122.0	1.7891	0.016213	192.94	192.95	-5.000	1024.5	1114.4	0.1680	1.7613	1.9293	122.0
124.0	1.8901	0.016221	183.23	183.24	-5.000	1023.3	1115.3	0.1715	1.7533	1.9247	124.0
126.0	1.9959	0.016229	174.08	174.09	-5.000	1022.2	1116.1	0.1749	1.7453	1.9202	126.0
128.0	2.1068	0.016238	165.45	165.47	-5.000	1021.0	1117.0	0.1783	1.7374	1.9157	128.0
130.0	2.2230	0.016247	157.32	157.33	-5.000	1019.8	1117.8	0.1817	1.7295	1.9112	130.0
132.0	2.3445	0.016256	149.64	149.66	-5.000	1018.7	1118.6	0.1851	1.7217	1.9068	132.0
134.0	2.4717	0.016265	142.40	142.41	-5.000	1017.5	1119.5	0.1884	1.7140	1.9024	134.0
136.0	2.6047	0.016274	135.55	135.57	-5.000	1016.4	1120.3	0.1918	1.7063	1.8980	136.0
138.0	2.7438	0.016284	129.09	129.11	-5.000	1015.2	1121.1	0.1951	1.6986	1.8937	138.0
140.0	2.8892	0.016293	122.98	123.00	-5.000	1014.0	1122.0	0.1985	1.6910	1.8895	140.0
142.0	3.0411	0.016303	117.21	117.22	-5.000	1012.9	1122.8	0.2018	1.6834	1.8852	142.0
144.0	3.1997	0.016312	111.74	111.76	-5.000	1011.7	1123.6	0.2051	1.6759	1.8810	144.0
146.0	3.3653	0.016322	106.58	106.59	-5.000	1010.5	1124.5	0.2084	1.6684	1.8769	146.0
148.0	3.5381	0.016332	101.68	101.70	-5.000	1009.3	1125.3	0.2117	1.6610	1.8727	148.0
150.0	3.7184	0.016343	97.05	97.07	-5.000	1008.2	1126.1	0.2150	1.6536	1.8686	150.0
152.0	3.9065	0.016353	92.66	92.68	-5.000	1007.0	1126.9	0.2183	1.6463	1.8646	152.0
154.0	4.1025	0.016363	88.50	88.52	-5.000	1005.8	1127.7	0.2216	1.6390	1.8606	154.0
156.0	4.3068	0.016374	84.56	84.57	-5.000	1004.6	1128.6	0.2248	1.6318	1.8566	156.0
158.0	4.5197	0.016384	80.82	80.83	-5.000	1003.4	1129.4	0.2281	1.6245	1.8526	158.0
160.0	4.7414	0.016395	77.27	77.29	-5.000	1002.2	1130.2	0.2313	1.6174	1.8487	160.0
162.0	4.9722	0.016406	73.90	73.92	-5.000	1001.0	1131.0	0.2345	1.6103	1.8448	162.0
164.0	5.2124	0.016417	70.70	70.72	-5.000	999.8	1131.8	0.2377	1.6032	1.8409	164.0
166.0	5.4623	0.016428	67.67	67.68	-5.000	998.6	1132.6	0.2409	1.5961	1.8371	166.0
168.0	5.7223	0.016440	64.78	64.80	-5.000	997.4	1133.4	0.2441	1.5892	1.8333	168.0
170.0	5.9925	0.016451	62.04	62.06	-5.000	996.2	1134.2	0.2473	1.5823	1.8295	170.0
172.0	6.2736	0.016463	59.43	59.45	-5.000	995.0	1135.0	0.2505	1.5753	1.8258	172.0
174.0	6.5656	0.016474	56.95	56.97	-5.000	993.8	1135.8	0.2537	1.5684	1.8221	174.0
176.0	6.8690	0.016486	54.59	54.61	-5.000	992.5	1136.6	0.2568	1.5616	1.8184	176.0
178.0	7.1840	0.016498	52.35	52.36	-5.000	991.4	1137.4	0.2600	1.5548	1.8147	178.0

Temp Fahr t	Abs Press Lb per Sq. In. p	Specific volume			Enthalpy			Entropy			Temp Fahr t
		Sat. Liquid v _l	Evap v _{fg}	Sat. Vapor v _g	Sat. Liquid h _l	Evap h _{fg}	Sat. Vapor h _g	Sat. Liquid s _l	Evap s _{fg}	Sat. Vapor s _g	
180.0	7.5110	0.016510	50.21	50.22	148.00	990.2	1138.2	0.2631	1.5480	1.8111	180.0
182.0	7.7653	0.016522	48.172	48.189	150.01	989.0	1139.0	0.2662	1.5413	1.8075	182.0
184.0	8.203	0.016534	46.232	46.249	152.01	987.8	1139.8	0.2694	1.5346	1.8040	184.0
186.0	8.566	0.016547	44.383	44.400	154.02	986.5	1140.5	0.2725	1.5279	1.8004	186.0
188.0	8.947	0.016559	42.621	42.638	156.03	985.3	1141.3	0.2756	1.5213	1.7969	188.0
190.0	9.340	0.016572	40.941	40.957	158.04	984.1	1142.1	0.2787	1.5148	1.7934	190.0
192.0	9.747	0.016585	39.337	39.354	160.05	982.8	1142.9	0.2818	1.5082	1.7900	192.0
194.0	10.166	0.016598	37.808	37.824	162.05	981.6	1143.7	0.2848	1.5017	1.7865	194.0
196.0	10.605	0.016611	36.348	36.364	164.06	980.4	1144.4	0.2879	1.4952	1.7831	196.0
198.0	11.058	0.016624	34.954	34.970	166.08	979.1	1145.2	0.2910	1.4888	1.7798	198.0
200.0	11.525	0.016637	33.622	33.639	168.09	977.9	1146.0	0.2940	1.4824	1.7764	200.0
204.0	12.512	0.016664	31.135	31.151	172.11	975.4	1147.5	0.3001	1.4697	1.7698	204.0
208.0	13.555	0.016691	28.862	28.878	176.14	972.8	1149.0	0.3061	1.4571	1.7632	208.0
212.0	14.655	0.016719	26.782	26.799	180.17	970.3	1150.5	0.3121	1.4447	1.7568	212.0
216.0	15.901	0.016747	24.878	24.894	184.20	967.8	1152.0	0.3181	1.4323	1.7505	216.0
220.0	17.186	0.016775	23.131	23.148	188.23	965.2	1153.4	0.3241	1.4201	1.7442	220.0
224.0	18.555	0.016805	21.529	21.545	192.27	962.6	1154.9	0.3300	1.4081	1.7380	224.0
228.0	20.015	0.016834	20.056	20.073	196.31	960.0	1156.3	0.3359	1.3961	1.7320	228.0
232.0	21.557	0.016864	18.701	18.718	200.35	957.4	1157.8	0.3417	1.3842	1.7260	232.0
236.0	23.215	0.016895	17.454	17.471	204.40	954.8	1159.2	0.3476	1.3725	1.7201	236.0
240.0	24.968	0.016926	16.304	16.321	208.45	952.1	1160.6	0.3533	1.3609	1.7142	240.0
244.0	26.826	0.016958	15.243	15.260	212.50	949.5	1162.0	0.3591	1.3494	1.7085	244.0
248.0	28.795	0.016990	14.264	14.281	216.56	946.8	1163.4	0.3649	1.3379	1.7028	248.0
252.0	30.883	0.017022	13.358	13.375	220.62	944.1	1164.7	0.3706	1.3266	1.6972	252.0
256.0	33.091	0.017055	12.520	12.538	224.69	941.4	1166.1	0.3763	1.3154	1.6917	256.0
260.0	35.427	0.017089	11.745	11.762	228.76	938.6	1167.4	0.3819	1.3043	1.6862	260.0
264.0	37.894	0.017123	11.025	11.042	232.83	935.9	1168.7	0.3876	1.2933	1.6808	264.0
268.0	40.500	0.017157	10.358	10.375	236.91	933.1	1170.0	0.3932	1.2823	1.6755	268.0
272.0	43.249	0.017193	9.738	9.755	240.99	930.3	1171.3	0.3987	1.2715	1.6702	272.0
276.0	46.147	0.017228	9.162	9.180	245.08	927.5	1172.5	0.4043	1.2607	1.6650	276.0
280.0	49.200	0.017264	8.627	8.644	249.17	924.6	1173.8	0.4098	1.2501	1.6599	280.0
284.0	52.414	0.017300	8.1280	8.1453	253.27	921.7	1175.0	0.4154	1.2395	1.6548	284.0
288.0	55.795	0.017334	7.6634	7.6807	257.37	918.8	1176.2	0.4208	1.2290	1.6498	288.0
292.0	59.350	0.017378	7.2301	7.2475	261.47	915.9	1177.4	0.4263	1.2186	1.6449	292.0
296.0	63.084	0.017411	6.8259	6.8433	265.56	913.0	1178.6	0.4317	1.2082	1.6400	296.0
300.0	67.005	0.01745	6.4483	6.4658	269.7	910.0	1179.7	0.4372	1.1979	1.6351	300.0
304.0	71.119	0.01749	6.0955	6.1130	273.8	907.0	1180.9	0.4426	1.1877	1.6303	304.0
308.0	75.433	0.01753	5.7655	5.7830	278.0	904.0	1182.0	0.4479	1.1776	1.6256	308.0
312.0	79.953	0.01757	5.4566	5.4742	282.1	901.0	1183.1	0.4533	1.1676	1.6209	312.0
316.0	84.688	0.01761	5.1673	5.1849	286.3	897.9	1184.1	0.4586	1.1576	1.6162	316.0
320.0	89.643	0.01766	4.8961	4.9138	290.4	894.8	1185.2	0.4640	1.1477	1.6116	320.0
324.0	94.826	0.01770	4.6418	4.6595	294.6	891.6	1186.2	0.4692	1.1378	1.6071	324.0
328.0	100.245	0.01774	4.4030	4.4208	298.7	888.5	1187.2	0.4745	1.1280	1.6025	328.0
332.0	105.907	0.01779	4.1788	4.1966	302.9	885.3	1188.2	0.4798	1.1183	1.5981	332.0
336.0	111.820	0.01783	3.9681	3.9859	307.1	882.1	1189.1	0.4850	1.1086	1.5936	336.0
340.0	117.992	0.01787	3.7699	3.7878	311.3	878.8	1190.1	0.4902	1.0990	1.5892	340.0
344.0	124.430	0.01792	3.5834	3.6013	315.5	875.5	1191.0	0.4954	1.0894	1.5849	344.0
348.0	131.142	0.01797	3.4078	3.4258	319.7	872.2	1191.1	0.5006	1.0799	1.5806	348.0
352.0	138.138	0.01801	3.2423	3.2603	323.9	868.9	1192.7	0.5058	1.0705	1.5763	352.0
356.0	145.424	0.01806	3.0863	3.1044	328.1	865.5	1193.6	0.5110	1.0611	1.5721	356.0
360.0	153.010	0.01811	2.9392	2.9573	332.3	862.1	1194.4	0.5161	1.0517	1.5678	360.0
364.0	160.903	0.01816	2.8002	2.8184	336.5	858.6	1195.2	0.5212	1.0424	1.5637	364.0
368.0	169.113	0.01821	2.6691	2.6873	340.8	855.1	1195.9	0.5263	1.0332	1.5595	368.0
372.0	177.648	0.01826	2.5451	2.5633	345.0	851.6	1196.7	0.5314	1.0240	1.5554	372.0
376.0	186.517	0.01831	2.4279	2.4462	349.3	848.1	1197.4	0.5365	1.0148	1.5513	376.0
380.0	195.729	0.01836	2.3170	2.3353	353.6	844.5	1198.0	0.5416	1.0057	1.5473	380.0
384.0	205.294	0.01842	2.2120	2.2304	357.9	840.8	1198.7	0.5466	0.9966	1.5432	384.0
388.0	215.220	0.01847	2.1126	2.1311	362.2	837.2	1199.3	0.5516	0.9876	1.5392	388.0
392.0	225.516	0.01853	2.0184	2.0369	366.5	833.4	1199.9	0.5567	0.9786	1.5352	392.0
396.0	236.193	0.01858	1.9291	1.9477	370.8	829.7	1200.4	0.5617	0.9696	1.5313	396.0
400.0	247.259	0.01864	1.8444	1.8630	375.1	825.9	1201.0	0.5667	0.9607	1.5274	400.0
404.0	258.725	0.01870	1.7640	1.7827	379.4	822.0	1201.5	0.5717	0.9518	1.5234	404.0
408.0	270.600	0.01875	1.6877	1.7064	383.7	818.2	1201.9	0.5766	0.9429	1.5195	408.0
412.0	282.894	0.01881	1.6152	1.6340	388.0	814.2	1202.4	0.5816	0.9341	1.5157	412.0
416.0	295.617	0.01887	1.5463	1.5651	392.5	810.2	1202.8	0.5866	0.9253	1.5118	416.0
420.0	308.780	0.01894	1.4808	1.4997	396.9	806.2	1203.1	0.5915	0.9165	1.5080	420.0
424.0	322.391	0.01900	1.4184	1.4374	401.3	802.2	1203.5	0.5964	0.9077	1.5042	424.0
428.0	336.463	0.01906	1.3591	1.3782	405.7	798.0	1203.7	0.6014	0.8990	1.5004	428.0
432.0	351.00	0.01913	1.30266	1.32179	410.1	793.9	1204.0	0.6063	0.8903	1.4966	432.0
436.0	366.03	0.01919	1.24887	1.26806	414.6	789.7	1204.2	0.6112	0.8816	1.4928	436.0
440.0	381.54	0.01926	1.19761	1.21687	419.0	785.4	1204.4	0.6161	0.8729	1.4890	440.0
444.0	397.56	0.01933	1.14874	1.16806	423.5	781.1	1204.6	0.6210	0.8643	1.4853	444.0
448.0	414.09	0.01940	1.10212	1.12152	428.0	776.7	1204.7	0.6259	0.8557	1.4815	448.0
452.0	431.14	0.01947	1.05764	1.07711	432.5	772.3	1204.8	0.6308	0.8471	1.4778	452.0
456.0	448.73	0.01954	1.01518	1.03472	437.0	767.8	1204.8	0.6356	0.8385	1.4741	456.0

Table 1. Saturated Steam: Temperature Table—Continued

Temp Fahr	Abs Press Lb per Sq In p	Specific Volume			Enthalpy			Entropy			Temp Fahr
		Sat. Liquid v _l	Evap v _{fg}	Sat. Vapor v _g	Sat. Liquid h _l	Evap h _{fg}	Sat. Vapor h _g	Sat. Liquid s _l	Evap s _{fg}	Sat. Vapor s _g	
460.0	466.87	0.01961	0.97463	0.99424	441.5	763.2	1204.8	0.6405	0.8299	1.4704	460.0
464.0	485.56	0.01969	0.93588	0.95557	446.1	758.6	1204.7	0.6454	0.8213	1.4667	464.0
468.0	504.83	0.01976	0.89885	0.91862	450.7	754.0	1204.6	0.6502	0.8127	1.4629	468.0
472.0	524.67	0.01984	0.86345	0.88329	455.2	749.3	1204.5	0.6551	0.8042	1.4592	472.0
476.0	545.11	0.01992	0.82958	0.84950	459.9	744.5	1204.3	0.6599	0.7956	1.4555	476.0
480.0	566.15	0.02000	0.79716	0.81717	464.5	739.6	1204.1	0.6648	0.7871	1.4518	480.0
484.0	587.81	0.02009	0.76613	0.78622	469.1	734.7	1203.8	0.6696	0.7785	1.4481	484.0
488.0	610.10	0.02017	0.73641	0.75658	473.8	729.7	1203.5	0.6745	0.7700	1.4444	488.0
492.0	633.03	0.02026	0.70794	0.72820	478.5	724.6	1203.1	0.6793	0.7614	1.4407	492.0
496.0	656.61	0.02034	0.68065	0.70100	483.2	719.5	1202.7	0.6842	0.7528	1.4370	496.0
500.0	680.86	0.02043	0.65448	0.67492	487.9	714.3	1202.2	0.6890	0.7443	1.4333	500.0
504.0	705.78	0.02053	0.62938	0.64991	492.7	709.0	1201.7	0.6939	0.7357	1.4296	504.0
508.0	731.40	0.02062	0.60530	0.62592	497.5	703.7	1201.1	0.6987	0.7271	1.4258	508.0
512.0	757.72	0.02072	0.58218	0.60289	502.3	698.2	1200.5	0.7036	0.7185	1.4221	512.0
516.0	784.76	0.02081	0.55997	0.58079	507.1	692.7	1199.8	0.7085	0.7099	1.4183	516.0
520.0	812.53	0.02091	0.53864	0.55956	512.0	687.0	1199.0	0.7133	0.7013	1.4146	520.0
524.0	841.04	0.02102	0.51814	0.53916	516.9	681.3	1198.2	0.7182	0.6926	1.4108	524.0
528.0	870.31	0.02112	0.49843	0.51955	521.8	675.5	1197.3	0.7231	0.6839	1.4070	528.0
532.0	900.34	0.02123	0.47947	0.50070	526.8	669.6	1196.4	0.7280	0.6752	1.4032	532.0
536.0	931.17	0.02134	0.46123	0.48257	531.7	663.6	1195.4	0.7329	0.6665	1.3993	536.0
540.0	962.79	0.02146	0.44367	0.46513	536.8	657.5	1194.3	0.7378	0.6577	1.3954	540.0
544.0	995.22	0.02157	0.42677	0.44834	541.8	651.3	1193.1	0.7427	0.6489	1.3915	544.0
548.0	1028.49	0.02169	0.41048	0.43217	546.9	645.0	1191.9	0.7476	0.6400	1.3876	548.0
552.0	1062.59	0.02182	0.39479	0.41660	552.0	638.5	1190.6	0.7525	0.6311	1.3837	552.0
556.0	1097.55	0.02194	0.37966	0.40160	557.2	632.0	1189.2	0.7575	0.6222	1.3797	556.0
560.0	1133.38	0.02207	0.36507	0.38714	562.4	625.3	1187.7	0.7625	0.6132	1.3757	560.0
564.0	1170.10	0.02221	0.35099	0.37320	567.6	618.5	1186.1	0.7674	0.6041	1.3716	564.0
568.0	1207.72	0.02235	0.33741	0.35975	572.9	611.5	1184.5	0.7725	0.5950	1.3675	568.0
572.0	1246.26	0.02249	0.32429	0.34678	578.3	604.5	1182.7	0.7775	0.5859	1.3634	572.0
576.0	1285.74	0.02264	0.31162	0.33426	583.7	597.2	1180.9	0.7825	0.5766	1.3592	576.0
580.0	1326.17	0.02279	0.29937	0.32216	589.1	589.9	1179.0	0.7876	0.5673	1.3550	580.0
584.0	1367.7	0.02295	0.28753	0.31048	594.6	582.4	1176.9	0.7927	0.5580	1.3507	584.0
588.0	1410.0	0.02311	0.27608	0.29919	600.1	574.7	1174.8	0.7978	0.5485	1.3464	588.0
592.0	1453.3	0.02328	0.26499	0.28827	605.7	566.8	1172.6	0.8030	0.5390	1.3420	592.0
596.0	1497.8	0.02345	0.25425	0.27770	611.4	558.8	1170.2	0.8082	0.5293	1.3375	596.0
600.0	1543.2	0.02364	0.24384	0.26747	617.1	550.6	1167.7	0.8134	0.5196	1.3330	600.0
604.0	1589.7	0.02382	0.23374	0.25757	622.9	542.2	1165.1	0.8187	0.5097	1.3284	604.0
608.0	1637.3	0.02402	0.22394	0.24796	628.8	533.6	1162.4	0.8240	0.4997	1.3238	608.0
612.0	1686.1	0.02422	0.21442	0.23865	634.8	524.7	1159.5	0.8294	0.4896	1.3190	612.0
616.0	1735.9	0.02444	0.20516	0.22960	640.8	515.6	1156.4	0.8348	0.4794	1.3141	616.0
620.0	1786.9	0.02466	0.19615	0.22081	646.9	506.3	1153.2	0.8403	0.4689	1.3092	620.0
624.0	1839.0	0.02489	0.18737	0.21226	653.1	496.6	1149.8	0.8458	0.4583	1.3041	624.0
628.0	1892.4	0.02514	0.17880	0.20394	659.5	486.7	1146.1	0.8514	0.4474	1.2988	628.0
632.0	1947.0	0.02539	0.17044	0.19583	665.9	476.4	1142.2	0.8571	0.4364	1.2934	632.0
636.0	2002.8	0.02566	0.16226	0.18792	672.4	465.7	1138.1	0.8628	0.4251	1.2879	636.0
640.0	2059.9	0.02595	0.15427	0.18021	679.1	454.6	1133.7	0.8686	0.4134	1.2821	640.0
644.0	2118.3	0.02625	0.14644	0.17259	685.9	443.1	1129.0	0.8746	0.4015	1.2761	644.0
648.0	2178.1	0.02657	0.13876	0.16534	692.9	431.1	1124.0	0.8806	0.3893	1.2699	648.0
652.0	2239.2	0.02691	0.13124	0.15816	700.0	418.7	1118.7	0.8868	0.3767	1.2634	652.0
656.0	2301.7	0.02728	0.12387	0.15115	707.4	405.7	1113.1	0.8931	0.3637	1.2567	656.0
660.0	2365.7	0.02768	0.11663	0.14431	714.9	392.1	1107.0	0.8995	0.3502	1.2498	660.0
664.0	2431.1	0.02811	0.10947	0.13757	722.9	377.7	1100.6	0.9064	0.3361	1.2425	664.0
668.0	2498.1	0.02858	0.10229	0.13087	731.5	362.1	1093.5	0.9137	0.3210	1.2347	668.0
672.0	2566.6	0.02911	0.09514	0.12424	740.2	345.7	1085.9	0.9212	0.3054	1.2266	672.0
676.0	2636.8	0.02970	0.08799	0.11769	749.2	328.5	1077.6	0.9287	0.2892	1.2179	676.0
680.0	2708.6	0.03037	0.08080	0.11117	758.5	310.1	1068.5	0.9365	0.2720	1.2086	680.0
684.0	2782.1	0.03114	0.07349	0.10463	768.2	290.2	1058.4	0.9447	0.2537	1.1984	684.0
688.0	2857.4	0.03204	0.06595	0.09799	778.8	268.2	1047.0	0.9535	0.2337	1.1872	688.0
692.0	2934.5	0.03313	0.05797	0.09110	790.5	243.1	1033.6	0.9634	0.2110	1.1744	692.0
696.0	3013.4	0.03455	0.04916	0.08371	804.4	212.8	1017.2	0.9749	0.1841	1.1591	696.0
700.0	3094.3	0.03662	0.03857	0.07519	822.4	172.7	995.2	0.9901	0.1490	1.1390	700.0
704.0	3135.5	0.03824	0.03173	0.06997	835.0	144.7	979.7	1.0006	0.1246	1.1252	704.0
708.0	3177.2	0.04108	0.02192	0.06300	854.2	102.0	956.2	1.0169	0.0876	1.1046	708.0
709.0	3199.3	0.04427	0.01304	0.05730	873.0	61.4	934.4	1.0329	0.0527	1.0856	709.0
709.47*	3208.2	0.05078	0.00000	0.05078	906.0	0.0	906.0	1.0612	0.0000	1.0612	709.47*

*Critical temperature

Table 3. Superheated Steam

Abs Press Lb/Sq In (Sat. Temp)		Sat. Water	Sat. Steam	Temperature — Degrees Fahrenheit													
				200	250	300	350	400	450	500	600	700	800	900	1000	1100	1200
1 (101.74)	Sh			98.26	148.26	198.26	248.26	298.26	348.26	398.26	498.26	598.26	698.26	798.26	898.26	998.26	1098.26
	v	0.01614	333.6	392.5	422.4	452.3	482.1	511.9	541.7	571.5	631.1	690.7	750.3	809.8	869.4	929.0	988.6
	s	69.73	1105.8	1150.2	1172.9	1195.7	1218.7	1241.8	1265.1	1288.6	1336.1	1384.5	1433.7	1483.8	1534.9	1586.8	1639.7
5 (162.24)	Sh			37.76	87.76	137.76	187.76	237.76	287.76	337.76	437.76	537.76	637.76	737.76	837.76	937.76	1037.76
	v	0.01641	73.53	78.14	84.21	90.24	96.25	102.24	108.23	114.21	126.15	138.08	150.01	161.94	173.86	185.78	197.70
	s	130.20	1131.1	1148.6	1171.7	1194.8	1218.0	1241.3	1264.7	1288.2	1335.9	1384.3	1433.6	1483.7	1534.7	1586.7	1639.6
10 (193.21)	Sh			6.79	56.79	106.79	156.79	206.79	256.79	306.79	406.79	506.79	606.79	706.79	806.79	906.79	1006.79
	v	0.01659	38.42	38.84	41.93	44.98	48.02	51.03	54.04	57.04	63.03	69.00	74.98	80.94	86.91	92.87	98.84
	s	161.26	1143.3	1146.6	1170.2	1193.7	1217.1	1240.6	1264.1	1287.8	1335.5	1384.0	1433.4	1483.7	1534.6	1586.6	1639.5
14.696 (212.00)	Sh			38.00	88.00	138.00	188.00	238.00	288.00	388.00	488.00	588.00	688.00	788.00	888.00	988.00	
	v	0.0167	26.799	28.42	30.52	32.55	34.67	36.72	38.77	42.86	46.93	51.00	55.06	59.13	63.19	67.25	
	s	180.17	1150.5	1168.8	1192.5	1216.3	1239.9	1263.6	1287.4	1335.2	1383.8	1433.2	1483.4	1534.4	1586.5	1639.4	
15 (213.03)	Sh			36.97	86.97	136.97	186.97	236.97	286.97	386.97	486.97	586.97	686.97	786.97	886.97	986.97	
	v	0.01673	26.290	27.837	29.899	31.959	33.963	35.977	37.985	41.986	45.978	49.964	53.946	57.926	61.905	65.882	
	s	181.21	1150.9	1168.7	1192.5	1216.2	1239.9	1263.6	1287.3	1335.2	1383.8	1433.2	1483.4	1534.4	1586.5	1639.4	
20 (227.96)	Sh			22.04	72.04	122.04	172.04	222.04	272.04	372.04	472.04	572.04	672.04	772.04	872.04	972.04	
	v	0.01683	20.087	20.788	22.356	23.900	25.428	26.946	28.457	31.466	34.465	37.458	40.447	43.435	46.420	49.405	
	s	196.27	1156.3	1167.1	1191.4	1215.4	1239.2	1263.0	1286.9	1334.9	1383.5	1432.9	1483.2	1534.3	1586.3	1639.3	
25 (240.07)	Sh			9.93	59.93	109.93	159.93	209.93	259.93	359.93	459.93	559.93	659.93	759.93	859.93	959.93	
	v	0.01693	16.301	16.558	17.829	19.076	20.307	21.527	22.740	25.153	27.557	29.954	32.348	34.740	37.130	39.518	
	s	208.52	1160.6	1165.6	1190.2	1214.5	1238.5	1262.5	1286.4	1334.6	1383.3	1432.7	1483.0	1534.2	1586.2	1639.2	
30 (250.34)	Sh			49.66	99.66	149.66	199.66	249.66	299.66	349.66	449.66	549.66	649.66	749.66	849.66	949.66	
	v	0.01701	13.744	14.810	15.859	16.892	17.914	18.929	20.945	22.951	24.952	26.949	28.943	30.936	32.927		
	s	218.93	1164.1	1189.0	1213.5	1237.8	1261.9	1285.9	1334.2	1383.0	1432.5	1482.8	1534.0	1586.1	1639.0		
35 (259.29)	Sh			40.71	90.71	140.71	190.71	240.71	290.71	340.71	440.71	540.71	640.71	740.71	840.71	940.71	
	v	0.01708	11.896	12.654	13.562	14.453	15.334	16.207	17.939	19.662	21.379	23.092	24.803	26.512	28.220		
	s	228.03	1167.1	1187.8	1212.7	1237.1	1261.3	1285.5	1333.9	1382.8	1432.3	1482.7	1533.9	1586.0	1638.9		
40 (267.25)	Sh			32.75	82.75	132.75	182.75	232.75	282.75	332.75	432.75	532.75	632.75	732.75	832.75	932.75	
	v	0.01715	10.497	11.036	11.838	12.624	13.398	14.165	15.685	17.195	18.699	20.199	21.697	23.194	24.689		
	s	236.14	1169.8	1186.6	1211.7	1236.4	1260.8	1285.0	1333.6	1382.5	1432.1	1482.5	1533.7	1585.8	1638.8		
45 (274.44)	Sh			25.56	75.56	125.56	175.56	225.56	275.56	325.56	425.56	525.56	625.56	725.56	825.56	925.56	
	v	0.01721	9.399	9.777	10.497	11.201	11.892	12.577	13.932	15.276	16.614	17.950	19.282	20.613	21.943		
	s	243.49	1172.1	1185.4	1210.4	1235.7	1260.2	1284.6	1333.3	1382.3	1431.9	1482.3	1533.6	1585.7	1638.7		
50 (281.02)	Sh			18.98	68.98	118.98	168.98	218.98	268.98	318.98	418.98	518.98	618.98	718.98	818.98	918.98	
	v	0.01727	8.514	9.769	9.424	10.062	10.688	11.306	12.529	13.741	14.947	16.150	17.350	18.549	19.746		
	s	250.21	1174.1	1184.1	1209.9	1234.9	1259.6	1284.1	1332.9	1382.0	1431.7	1482.2	1533.4	1585.6	1638.6		
55 (287.07)	Sh			12.93	62.93	112.93	162.93	212.93	262.93	312.93	412.93	512.93	612.93	712.93	812.93	912.93	
	v	0.01733	7.787	7.945	8.546	9.130	9.702	10.267	11.381	12.485	13.583	14.677	15.769	16.859	17.948		
	s	256.43	1176.0	1182.9	1208.9	1234.2	1259.1	1283.6	1332.6	1381.8	1431.5	1482.0	1533.3	1585.5	1638.5		
60 (292.71)	Sh			7.29	57.29	107.29	157.29	207.29	257.29	307.29	407.29	507.29	607.29	707.29	807.29	907.29	
	v	0.01738	7.174	7.257	7.915	8.354	8.881	9.400	10.425	11.438	12.446	13.450	14.452	15.452	16.450		
	s	262.21	1177.6	1191.6	1208.0	1233.5	1258.5	1283.2	1332.3	1381.5	1431.3	1481.8	1533.2	1585.3	1638.4		
65 (297.98)	Sh			2.02	52.02	102.02	152.02	202.02	252.02	302.02	402.02	502.02	602.02	702.02	802.02	902.02	
	v	0.01743	6.653	6.675	7.195	7.697	8.186	8.667	9.615	10.552	11.484	12.412	13.337	14.261	15.183		
	s	257.63	1179.1	1180.3	1207.0	1232.7	1257.9	1282.7	1331.9	1381.3	1431.1	1481.6	1533.0	1585.2	1638.3		
70 (302.93)	Sh			47.07	97.07	147.07	197.07	247.07	297.07	397.07	497.07	597.07	697.07	797.07	897.07		
	v	0.01748	6.205	6.664	7.133	7.590	8.039	8.922	9.793	10.659	11.522	12.382	13.240	14.097			
	s	272.74	1180.6	1206.0	1232.0	1257.3	1282.2	1331.6	1381.0	1430.9	1481.5	1532.9	1585.1	1638.2			
75 (307.61)	Sh			42.39	92.39	142.39	192.39	242.39	292.39	392.39	492.39	592.39	692.39	792.39	892.39		
	v	0.01753	5.814	6.204	6.645	7.074	7.494	8.320	9.135	9.945	10.750	11.553	12.355	13.155			
	s	277.56	1181.9	1205.4	1231.2	1256.7	1281.7	1331.3	1380.7	1430.7	1481.3	1532.7	1585.0	1638.1			

Sh = superheat, F
 v = specific volume, cu ft per lb
 h = enthalpy, Btu per lb
 s = entropy, Btu per R per lb

Table 3. Superheated Steam—Continued

Abs Press Lb/Sq In (Sat. Temp)	Sat Water	Sat Steam	Temperature—Degrees Fahrenheit													
			350	400	450	500	550	600	700	800	900	1000	1100	1200	1300	1400

Sh = superheat

v = enthalpy, Btu per lb

Table 3. Superheated Steam - Continued

Abs Press Lb/Sq In (Sat. Temp)	Sat Water	Sat Steam	Temperature - Degrees Fahrenheit														
			400	450	500	550	600	700	800	900	1000	1100	1200	1300	1400	1500	
210 (385.91)	Sh		14.09	64.09	114.09	164.09	214.09	314.09	414.09	514.09	614.09	714.09	814.09	914.09	1014.09	1114.09	
	v	0.01844	2.1822	2.2254	2.4181	2.5880	2.7504	2.9078	3.2137	3.5128	3.8080	4.1007	4.3915	4.6811	4.9695	5.2571	5.5440
	h	359.91	1199.0	1208.2	1239.2	1268.0	1295.3	1321.9	1373.7	1425.1	1476.7	1528.8	1581.6	1635.2	1689.6	1744.8	1800.8
220 (389.88)	Sh		10.12	60.12	110.12	160.12	210.12	310.12	410.12	510.12	610.12	710.12	810.12	910.12	1010.12	1110.12	
	v	0.01850	2.0863	2.1240	2.2999	2.4638	2.6199	2.7710	3.0642	3.3504	3.6327	3.9125	4.1905	4.4671	4.7426	5.0173	5.2913
	h	364.17	1199.6	1206.3	1237.8	1266.9	1294.5	1321.2	1373.2	1424.7	1476.3	1528.5	1581.4	1635.0	1689.4	1744.8	1800.6
230 (393.70)	Sh		6.30	56.30	106.30	156.30	206.30	306.30	406.30	506.30	606.30	706.30	806.30	906.30	1006.30	1106.30	
	v	0.01855	1.9985	2.0212	2.1919	2.3503	2.5008	2.6461	2.9276	3.2020	3.4726	3.7406	4.0068	4.2717	4.5355	4.7984	5.0606
	h	368.28	1200.1	1204.4	1236.3	1265.7	1293.6	1320.4	1372.7	1424.2	1476.0	1528.2	1581.1	1634.8	1689.3	1744.5	1800.5
240 (397.39)	Sh		2.61	52.61	102.61	152.61	202.61	302.61	402.61	502.61	602.61	702.61	802.61	902.61	1002.61	1102.61	
	v	0.01860	1.9177	1.9268	2.0928	2.2462	2.3915	2.5316	2.8024	3.0661	3.3259	3.5831	3.8385	4.0926	4.3456	4.5977	4.8492
	h	372.27	1200.6	1202.4	1234.9	1264.6	1292.7	1319.7	1372.1	1423.8	1475.6	1527.9	1580.9	1634.6	1689.1	1744.3	1800.4
250 (400.97)	Sh		49.03	99.03	149.03	199.03	299.03	399.03	499.03	599.03	699.03	799.03	899.03	999.03	1099.03		
	v	0.01865	1.8432	2.0016	2.1504	2.2909	2.4262	2.6872	2.9410	3.1909	3.4382	3.6837	3.9278	4.1709	4.4131	4.6546	
	h	376.14	1201.1	1233.4	1263.5	1291.8	1319.0	1371.6	1423.4	1475.3	1527.6	1580.6	1634.4	1688.9	1744.2	1800.2	
260 (404.44)	Sh		45.56	95.56	145.56	195.56	295.56	395.56	495.56	595.56	695.56	795.56	895.56	995.56	1095.56		
	v	0.01870	1.7742	1.9173	2.0619	2.1981	2.3289	2.5808	2.8256	3.0663	3.3044	3.5408	3.7758	4.0097	4.2427	4.4750	
	h	379.90	1201.5	1231.9	1262.4	1290.9	1318.2	1371.1	1423.0	1474.9	1527.3	1580.4	1634.2	1688.7	1744.0	1800.1	
270 (407.80)	Sh		42.20	92.20	142.20	192.20	292.20	392.20	492.20	592.20	692.20	792.20	892.20	992.20	1092.20		
	v	0.01875	1.7101	1.8391	1.9799	2.1121	2.2388	2.4824	2.7186	2.9509	3.1806	3.4084	3.6349	3.8603	4.0849	4.3087	
	h	383.56	1201.9	1230.4	1261.2	1290.0	1317.5	1370.5	1422.6	1474.6	1527.1	1580.1	1634.0	1688.5	1743.9	1800.0	
280 (411.07)	Sh		38.93	88.93	138.93	188.93	288.93	388.93	488.93	588.93	688.93	788.93	888.93	988.93	1088.93		
	v	0.01880	1.6505	1.7665	1.9037	2.0322	2.1551	2.3909	2.6194	2.8437	3.0655	3.2855	3.5042	3.7217	3.9384	4.1543	
	h	387.12	1202.3	1228.8	1260.0	1289.1	1316.8	1370.0	1422.1	1474.2	1526.8	1579.9	1633.8	1688.4	1743.7	1799.8	
290 (414.25)	Sh		35.75	85.75	135.75	185.75	285.75	385.75	485.75	585.75	685.75	785.75	885.75	985.75	1085.75		
	v	0.01885	1.5948	1.6988	1.8327	1.9578	2.0772	2.3058	2.5269	2.7440	2.9585	3.1711	3.3824	3.5926	3.8019	4.0106	
	h	390.60	1202.6	1227.3	1258.9	1288.1	1316.0	1369.5	1421.7	1473.9	1526.5	1579.6	1633.5	1688.2	1743.6	1799.7	
300 (417.35)	Sh		32.65	82.65	132.65	182.65	282.65	382.65	482.65	582.65	682.65	782.65	882.65	982.65	1082.65		
	v	0.01889	1.5427	1.6356	1.7665	1.8883	2.0044	2.2263	2.4407	2.6509	2.8585	3.0643	3.2688	3.4721	3.6746	3.8764	
	h	393.99	1202.9	1225.7	1257.7	1287.2	1315.2	1368.9	1421.3	1473.6	1526.2	1579.4	1633.3	1688.0	1743.4	1799.6	
310 (420.36)	Sh		29.64	79.64	129.64	179.64	279.64	379.64	479.64	579.64	679.64	779.64	879.64	979.64	1079.64		
	v	0.01894	1.4939	1.5763	1.7044	1.8233	1.9363	2.1520	2.3600	2.5638	2.7650	2.9644	3.1625	3.3594	3.5555	3.7509	
	h	397.30	1203.2	1224.1	1256.5	1286.3	1314.5	1368.4	1420.9	1473.2	1525.9	1579.2	1633.1	1687.8	1743.3	1799.4	
320 (423.31)	Sh		26.69	76.69	126.69	176.69	276.69	376.69	476.69	576.69	676.69	776.69	876.69	976.69	1076.69		
	v	0.01899	1.4480	1.5207	1.6462	1.7623	1.8725	2.0823	2.2843	2.4821	2.6774	2.8708	3.0628	3.2538	3.4438	3.6332	
	h	400.53	1203.4	1222.5	1255.2	1285.3	1313.7	1367.8	1420.5	1472.9	1525.6	1578.9	1632.9	1687.6	1743.1	1799.3	
330 (426.18)	Sh		23.82	73.82	123.82	173.82	273.82	373.82	473.82	573.82	673.82	773.82	873.82	973.82	1073.82		
	v	0.01903	1.4048	1.4684	1.5915	1.7050	1.8125	2.0168	2.2132	2.4054	2.5950	2.7828	2.9692	3.1545	3.3389	3.5227	
	h	403.70	1203.6	1220.9	1254.0	1284.4	1313.0	1367.3	1420.0	1472.5	1525.3	1578.7	1632.7	1687.5	1742.9	1799.2	
340 (428.99)	Sh		21.01	71.01	121.01	171.01	271.01	371.01	471.01	571.01	671.01	771.01	871.01	971.01	1071.01		
	v	0.01908	1.3640	1.4191	1.5399	1.6511	1.7561	1.9552	2.1463	2.3333	2.5175	2.7000	2.8811	3.0611	3.2401	3.4186	
	h	406.80	1203.8	1219.2	1252.8	1283.4	1312.2	1366.7	1419.6	1472.2	1525.0	1578.4	1632.5	1687.3	1742.8	1799.0	
350 (431.73)	Sh		18.27	68.27	118.27	168.27	268.27	368.27	468.27	568.27	668.27	768.27	868.27	968.27	1068.27		
	v	0.01912	1.3255	1.3725	1.4913	1.6002	1.7028	1.8970	2.0832	2.2652	2.4445	2.6219	2.7980	2.9730	3.1471	3.3205	
	h	409.83	1204.0	1217.5	1251.5	1282.4	1311.4	1366.2	1419.2	1471.8	1524.7	1578.2	1632.3	1687.1	1742.6	1798.9	
360 (434.41)	Sh		15.59	65.59	115.59	165.59	265.59	365.59	465.59	565.59	665.59	765.59	865.59	965.59	1065.59		
	v	0.01917	1.2991	1.3285	1.4454	1.5521	1.6525	1.8421	2.0237	2.2009	2.3755	2.5482	2.7196	2.8898	3.0592	3.2279	
	h	412.31	1204.1	1215.8	1250.3	1281.5	1310.6	1365.6	1418.7	1471.5	1524.4	1577.9	1632.1	1686.9	1742.5	1798.8	
380 (439.61)	Sh		10.39	60.39	110.39	160.39	260.39	360.39	460.39	560.39	660.39	760.39	860.39	960.39	1060.39		
	v	0.01925	1.2218	1.2472	1.3606	1.4635	1.5598	1.7410	1.9139	2.0825	2.2484	2.4124	2.5750	2.7366	2.8973	3.0572	
	h	418.59	1204.4	1212.4	1247.7	1279.5	1309.0	1364.5	1417.9	1470.8	1523.8	1577.4	1631.6	1686.5	1742.2	1798.5	

Sh = superheat, F
v = specific volume, cu ft per lb

h = enthalpy, Btu per lb
s = entropy, Btu per R per lb

Table 3. Superheated Steam - Continued

Abs Press Lb/Sq In. (Sat. Temp)	Sat. Water	Sat. Steam	Temperature - Degrees Fahrenheit														
			450	500	550	600	650	700	800	900	1000	1100	1200	1300	1400	1500	
400 (444.60)	Sh		5.40	55.40	105.40	155.40	205.40	255.40	355.40	455.40	555.40	655.40	755.40	855.40	955.40	1055.40	
	v	0.01934	1.1613	1.1738	1.2841	1.3836	1.4763	1.5646	1.6499	1.7315	1.9759	2.1339	2.2901	2.4450	2.5987	2.7515	2.9037
	s	0.6217	1.4847	1.4894	1.5282	1.5611	1.5901	1.6163	1.6406	1.6650	1.7255	1.7632	1.7988	1.8325	1.8647	1.8955	1.9250
420 (449.40)	Sh		60	50.60	100.60	150.60	200.60	250.60	350.60	450.60	550.60	650.60	750.60	850.60	950.60	1050.60	
	v	0.01942	1.1057	1.1071	1.2148	1.3113	1.4007	1.4856	1.5676	1.7258	1.8795	2.0304	2.1795	2.3273	2.4739	2.6196	2.7647
	s	0.6276	1.4802	1.4808	1.5206	1.5542	1.5835	1.6100	1.6345	1.6791	1.7197	1.7575	1.7932	1.8269	1.8591	1.8899	1.9195
440 (454.03)	Sh		45.97	95.97	145.97	195.97	245.97	345.97	445.97	545.97	645.97	745.97	845.97	945.97	1045.97		
	v	0.01950	1.0554	1.1517	1.2454	1.3319	1.4138	1.4926	1.5645	1.7918	1.9363	2.0790	2.2203	2.3605	2.4998	2.6384	
	s	0.6332	1.4759	1.5132	1.5474	1.5772	1.6040	1.6286	1.6734	1.7142	1.7521	1.7878	1.8216	1.8538	1.8847	1.9143	
460 (458.50)	Sh		41.50	91.50	141.50	191.50	241.50	341.50	441.50	541.50	641.50	741.50	841.50	941.50	1041.50		
	v	0.01959	1.0092	1.0939	1.1852	1.2691	1.3482	1.4242	1.5073	1.7117	1.8504	1.9872	2.1226	2.2569	2.3903	2.5230	
	s	0.6387	1.4718	1.5060	1.5409	1.5711	1.5982	1.6230	1.6580	1.7089	1.7469	1.7826	1.8165	1.8488	1.8797	1.9093	
480 (462.82)	Sh		37.18	87.18	137.18	187.18	237.18	337.18	437.18	537.18	637.18	737.18	837.18	937.18	1037.18		
	v	0.01967	0.9668	1.0409	1.1300	1.2115	1.2881	1.3615	1.5023	1.6384	1.7716	1.9030	2.0330	2.1619	2.2900	2.4173	
	s	0.6439	1.4677	1.4990	1.5346	1.5652	1.5925	1.6176	1.6628	1.7038	1.7419	1.7777	1.8116	1.8439	1.8748	1.9045	
500 (467.01)	Sh		32.99	82.99	132.99	182.99	232.99	332.99	432.99	532.99	632.99	732.99	832.99	932.99	1032.99		
	v	0.01975	0.9276	0.9919	1.0791	1.1584	1.2327	1.3037	1.4397	1.5708	1.6992	1.8256	1.9507	2.0746	2.1977	2.3200	
	s	0.6490	1.4639	1.4921	1.5284	1.5595	1.5871	1.6123	1.6578	1.6990	1.7371	1.7730	1.8069	1.8393	1.8702	1.8998	
520 (471.07)	Sh		28.93	78.93	128.93	178.93	228.93	328.93	428.93	528.93	628.93	728.93	828.93	928.93	1028.93		
	v	0.01982	0.8914	0.9466	1.0321	1.1094	1.1816	1.2504	1.3819	1.5085	1.6323	1.7542	1.8746	1.9940	2.1125	2.2302	
	s	0.6540	1.4601	1.4853	1.5223	1.5539	1.5818	1.6072	1.6530	1.6943	1.7325	1.7684	1.8024	1.8348	1.8657	1.8954	
540 (475.01)	Sh		24.99	74.99	124.99	174.99	224.99	324.99	424.99	524.99	624.99	724.99	824.99	924.99	1024.99		
	v	0.01990	0.8577	0.9045	0.9884	1.0640	1.1342	1.2010	1.3284	1.4508	1.5704	1.6880	1.8042	1.9193	2.0336	2.1471	
	s	0.6587	1.4565	1.4786	1.5164	1.5485	1.5767	1.6023	1.6483	1.6897	1.7280	1.7640	1.7981	1.8305	1.8615	1.8911	
560 (478.84)	Sh		21.16	71.16	121.16	171.16	221.16	321.16	421.16	521.16	621.16	721.16	821.16	921.16	1021.16		
	v	0.01998	0.8264	0.8653	0.9479	1.0217	1.0902	1.1552	1.2787	1.3972	1.5129	1.6266	1.7388	1.8500	1.9603	2.0699	
	s	0.6634	1.4529	1.4720	1.5106	1.5431	1.5717	1.5975	1.6438	1.6853	1.7237	1.7598	1.7939	1.8263	1.8573	1.8870	
580 (482.57)	Sh		17.43	67.43	117.43	167.43	217.43	317.43	417.43	517.43	617.43	717.43	817.43	917.43	1017.43		
	v	0.02006	0.7971	0.8287	0.9100	0.9824	1.0492	1.1125	1.2324	1.3473	1.4593	1.5693	1.6780	1.7855	1.8921	1.9980	
	s	0.6679	1.4495	1.4654	1.5049	1.5380	1.5668	1.5929	1.6394	1.6811	1.7196	1.7556	1.7898	1.8223	1.8533	1.8831	
600 (486.20)	Sh		13.80	63.80	113.80	163.80	213.80	313.80	413.80	513.80	613.80	713.80	813.80	913.80	1013.80		
	v	0.02013	0.7697	0.7944	0.8746	0.9456	1.0109	1.0726	1.1922	1.3008	1.4093	1.5160	1.6211	1.7252	1.8284	1.9309	
	s	0.6723	1.4461	1.4590	1.4993	1.5329	1.5621	1.5884	1.6351	1.6769	1.7155	1.7517	1.7859	1.8184	1.8494	1.8792	
650 (494.89)	Sh		5.11	55.11	105.11	155.11	205.11	305.11	405.11	505.11	605.11	705.11	805.11	905.11	1005.11		
	v	0.02032	0.7084	0.7173	0.7954	0.8632	0.9254	0.9835	1.0929	1.1969	1.2979	1.3969	1.4944	1.5909	1.6864	1.7813	
	s	0.6828	1.4381	1.4430	1.4858	1.5207	1.5507	1.5775	1.6249	1.6671	1.7059	1.7422	1.7765	1.8092	1.8403	1.8701	
700 (503.08)	Sh		46.92	96.92	146.92	196.92	246.92	346.92	446.92	546.92	646.92	746.92	846.92	946.92	1046.92		
	v	0.02050	0.6556	0.7271	0.7928	0.8520	0.9072	1.0102	1.1078	1.2023	1.2948	1.3858	1.4757	1.5647	1.6530		
	s	0.6928	1.4304	1.4426	1.5090	1.5599	1.6073	1.6514	1.7037	1.7544	1.8033	1.8506	1.8964	1.9407	1.9839		
750 (510.84)	Sh		39.16	89.16	139.16	189.16	239.16	339.16	439.16	539.16	639.16	739.16	839.16	939.16	1039.16		
	v	0.02069	0.6095	0.6676	0.7313	0.7907	0.8409	0.9386	1.0306	1.1195	1.2063	1.2916	1.3759	1.4592	1.5419		
	s	0.7022	1.4232	1.4369	1.4977	1.5495	1.6029	1.6577	1.7150	1.7658	1.8186	1.8722	1.9258	1.9783	2.0298		
800 (518.21)	Sh		31.79	81.79	131.79	181.79	231.79	331.79	431.79	531.79	631.79	731.79	831.79	931.79	1031.79		
	v	0.02087	0.5690	0.6151	0.6774	0.7352	0.7828	0.8759	0.9631	1.0470	1.1289	1.2093	1.2885	1.3669	1.4446		
	s	0.7111	1.4163	1.4272	1.4869	1.5393	1.5934	1.6484	1.7053	1.7641	1.8249	1.8876	1.9522	2.0187	2.0871		
850 (525.24)	Sh		24.76	74.76	124.76	174.76	224.76	324.76	424.76	524.76	624.76	724.76	824.76	924.76	1024.76		
	v	0.02105	0.5330	0.5683	0.6296	0.6879	0.7315	0.8205	0.9034	0.9830	1.0606	1.1366	1.2115	1.2855	1.3588		
	s	0.7197	1.4095	1.4203	1.4763	1.5282	1.5816	1.6366	1.6934	1.7520	1.8124	1.8746	1.9386	2.0044	2.0721		
900 (531.95)	Sh		18.05	68.05	118.05	168.05	218.05	318.05	418.05	518.05	618.05	718.05	818.05	918.05	1018.05		
	v	0.02123	0.5009	0.5263	0.5869	0.6423	0.6858	0.7713	0.8504	0.9262	0.9998	1.0720	1.1430	1.2131	1.2825		
	s	0.7279	1.4032	1.4143	1.4689	1.5202	1.5731	1.6277	1.6841	1.7422	1.8020	1.8634	1.9264	1.9911	2.0575		

Sh = superheat, F
v = specific volume, cu ft per lb

h = enthalpy, Btu per lb
s = entropy, Btu per R per lb

Table 3. Superheated Steam - Continued

Abs Press Lb/Sq in (Sat. Temp)	Sat Water	Sat Steam	Temperature - Degrees Fahrenheit													
			550	600	650	700	750	800	850	900	1000	1100	1200	1300	1400	1500
950 (538.39)	Sh		11.51	61.61	111.61	161.61	211.61	261.61	311.61	361.61	461.61	561.61	661.61	761.61	861.61	961.61
	v	0.02141	0.4721	0.4883	0.5485	0.5993	0.6449	0.6871	0.7272	0.7656	0.8030	0.8753	0.9455	1.0142	1.0817	1.1484
	s	0.7358	1.3970	1.4098	1.4557	1.4921	1.5228	1.5500	1.5748	1.5977	1.6193	1.6595	1.6967	1.7317	1.7649	1.7965
1000 (544.58)	Sh		5.42	55.42	105.42	155.42	205.42	255.42	305.42	355.42	455.42	555.42	655.42	755.42	855.42	955.42
	v	0.02159	0.4460	0.4535	0.5137	0.5636	0.6080	0.6489	0.6875	0.7245	0.7603	0.8295	0.8966	0.9622	1.0266	1.0901
	s	0.7434	1.3910	1.3973	1.4457	1.4833	1.5149	1.5426	1.5677	1.5908	1.6126	1.6530	1.6905	1.7256	1.7589	1.7905
1050 (550.53)	Sh		49.47	99.47	149.47	199.47	249.47	299.47	349.47	399.47	449.47	549.47	649.47	749.47	849.47	949.47
	v	0.02177	0.4222	0.4821	0.5312	0.5745	0.6142	0.6515	0.6872	0.7216	0.7881	0.8524	0.9151	0.9767	1.0373	1.0973
	s	0.7507	1.3851	1.4358	1.4748	1.5072	1.5354	1.5608	1.5842	1.6062	1.6269	1.6469	1.6845	1.7197	1.7531	1.7848
1100 (556.28)	Sh		43.72	93.72	143.72	193.72	243.72	293.72	343.72	393.72	443.72	543.72	643.72	743.72	843.72	943.72
	v	0.02195	0.4006	0.4531	0.5017	0.5440	0.5826	0.6188	0.6533	0.6865	0.7505	0.8121	0.8723	0.9313	0.9894	1.0468
	s	0.7578	1.3794	1.4259	1.4664	1.4996	1.5284	1.5542	1.5779	1.6000	1.6210	1.6410	1.6787	1.7141	1.7475	1.7793
1150 (561.82)	Sh		39.18	89.18	139.18	189.18	239.18	289.18	339.18	389.18	439.18	539.18	639.18	739.18	839.18	939.18
	v	0.02214	0.3807	0.4263	0.4746	0.5162	0.5538	0.5889	0.6223	0.6544	0.7161	0.7754	0.8332	0.8899	0.9456	1.0007
	s	0.7647	1.3738	1.4160	1.4582	1.4923	1.5216	1.5478	1.5717	1.5941	1.6353	1.6732	1.7087	1.7422	1.7741	1.8045
1200 (567.19)	Sh		32.81	82.81	132.81	182.81	232.81	282.81	332.81	382.81	432.81	532.81	632.81	732.81	832.81	932.81
	v	0.02232	0.3624	0.4016	0.4497	0.4905	0.5273	0.5615	0.5939	0.6250	0.6845	0.7418	0.7974	0.8519	0.9055	0.9584
	s	0.7714	1.3683	1.4061	1.4501	1.4851	1.5150	1.5415	1.5658	1.5883	1.6298	1.6679	1.7035	1.7371	1.7691	1.7996
1300 (577.42)	Sh		22.58	72.58	122.58	172.58	222.58	272.58	322.58	372.58	422.58	522.58	622.58	722.58	822.58	922.58
	v	0.02269	0.3299	0.3570	0.4052	0.4451	0.4804	0.5129	0.5436	0.5729	0.6287	0.6822	0.7341	0.7847	0.8345	0.8836
	s	0.7843	1.3577	1.3860	1.4340	1.4711	1.5022	1.5296	1.5544	1.5773	1.6194	1.6578	1.6937	1.7275	1.7596	1.7902
1400 (587.07)	Sh		12.93	62.93	112.93	162.93	212.93	262.93	312.93	362.93	412.93	512.93	612.93	712.93	812.93	912.93
	v	0.02307	0.3018	0.3176	0.3667	0.4059	0.4400	0.4712	0.5004	0.5282	0.5809	0.6311	0.6798	0.7272	0.7737	0.8195
	s	0.7966	1.3474	1.1941	1.2514	1.2961	1.3345	1.3693	1.4020	1.4332	1.4932	1.5518	1.6099	1.6680	1.7263	1.7850
1500 (596.20)	Sh		3.80	53.80	103.80	153.80	203.80	253.80	303.80	353.80	403.80	503.80	603.80	703.80	803.80	903.80
	v	0.02346	0.2772	0.2820	0.3328	0.3717	0.4049	0.4350	0.4629	0.4894	0.5394	0.5869	0.6327	0.6773	0.7210	0.7639
	s	0.8085	1.3373	1.1763	1.2402	1.2879	1.3280	1.3640	1.3974	1.4292	1.4901	1.5492	1.6077	1.6662	1.7248	1.7837
1600 (604.87)	Sh		45.13	95.13	145.13	195.13	245.13	295.13	345.13	395.13	445.13	545.13	645.13	745.13	845.13	945.13
	v	0.02387	0.2555	0.3026	0.3415	0.3741	0.4032	0.4301	0.4555	0.5031	0.5482	0.5915	0.6336	0.6748	0.7153	
	s	0.8199	1.3274	1.2283	1.2794	1.3214	1.3585	1.3928	1.4252	1.4869	1.5469	1.6056	1.6633	1.7212	1.7793	
1700 (613.13)	Sh		36.87	86.87	136.87	186.87	236.87	286.87	336.87	386.87	436.87	536.87	636.87	736.87	836.87	936.87
	v	0.02428	0.2361	0.2754	0.3147	0.3468	0.3751	0.4011	0.4255	0.4711	0.5140	0.5552	0.5951	0.6341	0.6724	
	s	0.8309	1.3176	1.2153	1.2705	1.3145	1.3529	1.3881	1.4212	1.4838	1.5440	1.6034	1.6625	1.7217	1.7810	
1800 (621.02)	Sh		28.98	78.98	128.98	178.98	228.98	278.98	328.98	378.98	428.98	528.98	628.98	728.98	828.98	928.98
	v	0.02472	0.2186	0.2505	0.2906	0.3223	0.3500	0.3752	0.3988	0.4426	0.4836	0.5229	0.5609	0.5980	0.6343	
	s	0.8417	1.3079	1.2012	1.2611	1.3074	1.3472	1.3833	1.4171	1.4806	1.5414	1.6012	1.6607	1.7201	1.7797	
1900 (628.56)	Sh		21.44	71.44	121.44	171.44	221.44	271.44	321.44	371.44	421.44	521.44	621.44	721.44	821.44	921.44
	v	0.02517	0.2028	0.2274	0.2687	0.3004	0.3275	0.3521	0.3749	0.4171	0.4565	0.4940	0.5303	0.5656	0.6002	
	s	0.8522	1.2981	1.1957	1.2513	1.3002	1.3414	1.3784	1.4129	1.4774	1.5388	1.5991	1.6588	1.7186	1.7784	
2000 (635.80)	Sh		14.20	64.20	114.20	164.20	214.20	264.20	314.20	364.20	414.20	514.20	614.20	714.20	814.20	914.20
	v	0.02565	0.1883	0.2056	0.2488	0.2805	0.3072	0.3312	0.3534	0.3942	0.4320	0.4680	0.5027	0.5365	0.5695	
	s	0.8625	1.2881	1.1683	1.2409	1.2926	1.3354	1.3735	1.4087	1.4741	1.5362	1.5969	1.6570	1.7171	1.7771	
2100 (642.76)	Sh		7.04	57.04	107.04	157.04	207.04	257.04	307.04	357.04	407.04	507.04	607.04	707.04	807.04	907.04
	v	0.02615	0.1750	0.1847	0.2304	0.2624	0.2888	0.3123	0.3339	0.3734	0.4099	0.4445	0.4778	0.5101	0.5418	
	s	0.8727	1.2730	1.1485	1.2293	1.2749	1.3239	1.3684	1.4044	1.4709	1.5336	1.5947	1.6552	1.7154	1.7757	
2200 (649.45)	Sh		5.55	50.55	100.55	150.55	200.55	250.55	300.55	350.55	400.55	500.55	600.55	700.55	800.55	900.55
	v	0.02669	0.1627	0.1636	0.2134	0.2456	0.2720	0.2950	0.3161	0.3545	0.3897	0.4231	0.4551	0.4862	0.5165	
	s	0.8828	1.2576	1.1239	1.2190	1.2638	1.3123	1.3553	1.4000	1.4676	1.5309	1.5925	1.6533	1.7139	1.7744	
2300 (655.89)	Sh		4.11	44.11	94.11	144.11	194.11	244.11	294.11	344.11	394.11	444.11	544.11	644.11	744.11	844.11
	v	0.02727	0.1513	0.1518	0.2059	0.2385	0.2656	0.2893	0.3111	0.3497	0.3851	0.4181	0.4495	0.4795	0.5085	
	s	0.8929	1.2369	1.1059	1.2053	1.2544	1.3067	1.3531	1.3957	1.4642	1.5283	1.5903	1.6515	1.7123	1.7731	

Sh = superheat, F

v = specific volume, cu ft per lb

h = enthalpy, Btu per lb

s = entropy, Btu per R per lb

Table 3. Superheated Steam - Continued

Abs. Press. Lb./Sq. in. (Sat. Temp.)	Sat. Water	Sat. Steam	Temperature - Degrees Fahrenheit														
			700	750	800	850	900	950	1000	1050	1100	1150	1200	1300	1400	1500	
2400 (662.11)	Sh		17.39	87.89	137.89	187.89	237.89	287.89	337.89	387.89	437.89	487.89	537.89	637.89	737.89	837.89	
	v	0.02790	0.1408	0.1604	0.2164	0.2424	0.2648	0.2850	0.3037	0.3214	0.3382	0.3545	0.3703	0.3856	0.4155	0.4443	0.4724
	s	0.9031	1.2460	1.3022	1.3808	1.4217	1.4549	1.4837	1.5095	1.5332	1.5553	1.5761	1.5959	1.6149	1.6509	1.6847	1.7167
2500 (668.11)	Sh		17.39	81.89	131.89	181.89	231.89	281.89	331.89	381.89	431.89	481.89	531.89	631.89	731.89	831.89	
	v	0.02859	0.1307	0.1551	0.2032	0.2293	0.2514	0.2712	0.2896	0.3066	0.3230	0.3383	0.3543	0.3692	0.3980	0.4259	0.4529
	s	0.9139	1.2345	1.3076	1.3701	1.4129	1.4472	1.4766	1.5029	1.5269	1.5492	1.5703	1.5903	1.6094	1.6456	1.6796	1.7116
2600 (673.91)	Sh		16.09	76.09	126.09	176.09	226.09	276.09	326.09	376.09	426.09	476.09	526.09	626.09	726.09	826.09	
	v	0.02938	0.1211	0.1455	0.1909	0.2171	0.2390	0.2585	0.2765	0.2933	0.3093	0.3247	0.3395	0.3540	0.3819	0.4088	0.4350
	s	0.9247	1.2225	1.3008	1.3592	1.4042	1.4395	1.4696	1.4964	1.5208	1.5434	1.5646	1.5848	1.6040	1.6405	1.6746	1.7068
2700 (679.53)	Sh		15.07	70.47	120.47	170.47	220.47	270.47	320.47	370.47	420.47	470.47	520.47	620.47	720.47	820.47	
	v	0.03029	0.1119	0.1363	0.1794	0.2058	0.2275	0.2468	0.2644	0.2809	0.2965	0.3114	0.3259	0.3399	0.3670	0.3931	0.4184
	s	0.9356	1.2097	1.2877	1.3481	1.3954	1.4319	1.4628	1.4900	1.5148	1.5376	1.5591	1.5794	1.5988	1.6355	1.6697	1.7021
2800 (684.96)	Sh		15.04	65.04	115.04	165.04	215.04	265.04	315.04	365.04	415.04	465.04	515.04	615.04	715.04	815.04	
	v	0.03134	0.1030	0.1273	0.1685	0.1952	0.2168	0.2358	0.2531	0.2693	0.2845	0.2991	0.3132	0.3268	0.3532	0.3785	0.4030
	s	0.9468	1.1958	1.2727	1.3368	1.3867	1.4245	1.4561	1.4838	1.5089	1.5321	1.5537	1.5742	1.5938	1.6306	1.6651	1.6975
2900 (690.22)	Sh		14.78	59.78	109.78	159.78	209.78	259.78	309.78	359.78	409.78	459.78	509.78	609.78	709.78	809.78	
	v	0.03262	0.0942	0.1183	0.1581	0.1853	0.2068	0.2256	0.2427	0.2585	0.2734	0.2877	0.3014	0.3147	0.3403	0.3649	0.3887
	s	0.9588	1.1803	1.2573	1.3251	1.3780	1.4171	1.4494	1.4777	1.5032	1.5266	1.5485	1.5692	1.5889	1.6259	1.6605	1.6931
3000 (695.33)	Sh		14.67	54.67	104.67	154.67	204.67	254.67	304.67	354.67	404.67	454.67	504.67	604.67	704.67	804.67	
	v	0.03428	0.0850	0.0982	0.1483	0.1759	0.1975	0.2161	0.2329	0.2484	0.2630	0.2770	0.2904	0.3033	0.3282	0.3522	0.3753
	s	0.9728	1.1619	1.2366	1.3131	1.3692	1.4097	1.4429	1.4717	1.4976	1.5213	1.5434	1.5642	1.5841	1.6214	1.6561	1.6888
3100 (700.28)	Sh		14.72	49.72	99.72	149.72	199.72	249.72	299.72	349.72	399.72	449.72	499.72	599.72	699.72	799.72	
	v	0.03681	0.0745	0.1389	0.1671	0.1887	0.2071	0.2237	0.2390	0.2533	0.2670	0.2800	0.2927	0.3170	0.3403	0.3628	
	s	0.9914	1.1373	1.3007	1.3604	1.4024	1.4364	1.4658	1.4920	1.5161	1.5384	1.5594	1.5794	1.6169	1.6518	1.6847	
3200 (705.08)	Sh		44.92	94.92	144.92	194.92	244.92	294.92	344.92	394.92	444.92	494.92	594.92	694.92	794.92		
	v	0.04472	0.0566	0.1300	0.1588	0.1804	0.1987	0.2151	0.2301	0.2442	0.2576	0.2704	0.2827	0.3065	0.3291	0.3510	
	s	1.0351	1.0832	1.2877	1.3515	1.3951	1.4300	1.4600	1.4866	1.5110	1.5335	1.5547	1.5749	1.6126	1.6477	1.6806	
3300	Sh		0.1213	0.1510	0.1727	0.1908	0.2070	0.2218	0.2357	0.2488	0.2613	0.2734	0.2966	0.3187	0.3400		
	v		1.158.2	1.242.5	1.300.7	1.348.4	1.390.7	1.429.5	1.466.1	1.501.0	1.534.9	1.568.1	1.632.9	1.696.7	1.759.9		
	s		1.274.2	1.342.5	1.387.9	1.423.7	1.454.2	1.481.3	1.505.9	1.528.7	1.550.1	1.570.4	1.608.4	1.643.6	1.676.7		
3400	Sh		0.1129	0.1435	0.1653	0.1834	0.1994	0.2140	0.2276	0.2405	0.2528	0.2646	0.2872	0.3088	0.3296		
	v		1.143.2	1.233.7	1.294.3	1.343.4	1.386.4	1.425.9	1.462.9	1.498.3	1.532.4	1.565.8	1.631.1	1.695.1	1.758.5		
	s		1.260.0	1.333.4	1.380.7	1.417.4	1.448.6	1.476.1	1.501.0	1.524.0	1.545.6	1.566.0	1.604.2	1.639.6	1.672.8		
3500	Sh		0.1048	0.1364	0.1583	0.1764	0.1922	0.2066	0.2200	0.2326	0.2447	0.2563	0.2784	0.2995	0.3198		
	v		1.127.1	1.224.6	1.287.8	1.338.2	1.382.2	1.422.2	1.459.7	1.495.5	1.529.9	1.563.6	1.629.2	1.693.6	1.757.2		
	s		1.245.0	1.324.2	1.373.4	1.411.2	1.443.0	1.470.9	1.496.2	1.519.4	1.541.2	1.561.8	1.600.2	1.635.8	1.669.1		
3600	Sh		0.0966	0.1296	0.1517	0.1697	0.1854	0.1996	0.2128	0.2252	0.2371	0.2485	0.2702	0.2908	0.3106		
	v		1.108.6	1.215.3	1.281.2	1.333.0	1.377.9	1.418.6	1.456.5	1.492.6	1.527.4	1.561.3	1.627.3	1.692.0	1.755.9		
	s		1.228.1	1.314.8	1.366.2	1.405.0	1.437.4	1.465.8	1.491.4	1.514.9	1.536.9	1.557.6	1.596.2	1.632.0	1.665.4		
3800	Sh		0.0799	0.1169	0.1395	0.1574	0.1729	0.1868	0.1996	0.2116	0.2231	0.2340	0.2549	0.2746	0.2936		
	v		1.064.2	1.195.5	1.267.5	1.322.4	1.369.1	1.411.2	1.450.1	1.487.0	1.522.4	1.556.8	1.623.6	1.688.9	1.753.2		
	s		1.188.8	1.295.5	1.351.7	1.392.8	1.426.5	1.455.8	1.482.1	1.506.1	1.528.4	1.549.5	1.588.6	1.624.7	1.658.4		
4000	Sh		0.0631	0.1052	0.1284	0.1463	0.1616	0.1752	0.1877	0.1994	0.2105	0.2210	0.2411	0.2601	0.2783		
	v		1.007.4	1.174.3	1.255.4	1.311.5	1.360.2	1.403.6	1.443.6	1.481.3	1.517.3	1.552.2	1.619.8	1.685.7	1.750.6		
	s		1.139.6	1.275.4	1.337.7	1.380.7	1.415.8	1.446.1	1.473.0	1.497.6	1.520.3	1.541.7	1.581.2	1.617.7	1.651.6		
4200	Sh		0.0498	0.0945	0.1183	0.1362	0.1513	0.1647	0.1769	0.1883	0.1991	0.2093	0.2287	0.2474	0.2645		
	v		0.950.1	1.131.6	1.235.6	1.300.4	1.351.2	1.399.0	1.437.1	1.475.5	1.512.2	1.547.6	1.616.1	1.682.6	1.748.0		
	s		1.090.5	1.254.4	1.327.3	1.366.6	1.405.3	1.436.6	1.464.2	1.489.3	1.512.3	1.534.1	1.574.2	1.610.9	1.645.2		
4400	Sh		0.0421	0.0846	0.1090	0.1272	0.1420	0.1552	0.1671	0.1782	0.1887	0.1986	0.2174	0.2351	0.2519		
	v		0.909.5	1.117.3	1.233.3	1.299.0	1.345.0	1.383.3	1.413.4	1.446.7	1.479.1	1.510.4	1.543.0	1.612.3	1.745.3		
	s		1.055.6	1.235.5	1.307.8	1.356.6	1.394.9	1.427.2	1.455.6	1.481.2	1.504.8	1.526.8	1.567.3	1.604.4	1.638.9		

Sh = superheat F
v = specific volume, cu ft per lb

h = enthalpy, Btu per lb
s = entropy, Btu per R per lb

Table 3. Superheated Steam - Continued

Abs Press. Lb/Sq In (Sat. Temp)	Sat Water	Sat Steam	Temperature - Degrees Fahrenheit													
			750	800	850	900	950	1000	1050	1100	1150	1200	1250	1300	1400	1500
4600			0.0380	0.0751	0.1005	0.1186	0.1335	0.1465	0.1582	0.1691	0.1792	0.1889	0.1982	0.2071	0.2242	0.2404
			883.8	1100.0	1207.3	1277.2	1332.5	1380.5	1423.7	1463.9	1501.9	1538.4	1573.8	1608.5	1676.3	1742.7
			0.9331	1.2084	1.2922	1.3426	1.3847	1.4181	1.4472	1.4734	1.4974	1.5197	1.5407	1.5607	1.5982	1.6330
4800			0.0355	0.0665	0.0927	0.1109	0.1257	0.1385	0.1500	0.1606	0.1706	0.1800	0.1890	0.1977	0.2142	0.2299
			866.9	1071.2	1190.7	1255.2	1323.1	1372.6	1417.0	1458.0	1496.7	1533.8	1569.7	1604.7	1673.1	1740.0
			0.9180	1.1835	1.2768	1.3227	1.3745	1.4090	1.4390	1.4657	1.4901	1.5128	1.5341	1.5543	1.5921	1.6272
5000			0.0338	0.0591	0.0855	0.1038	0.1185	0.1312	0.1425	0.1529	0.1626	0.1718	0.1806	0.1890	0.2050	0.2203
			854.9	1042.9	1173.6	1252.9	1313.5	1364.6	1410.2	1452.1	1491.5	1529.1	1565.5	1600.9	1670.0	1737.4
			0.9070	1.1593	1.2612	1.3207	1.3645	1.4001	1.4309	1.4582	1.4831	1.5061	1.5277	1.5481	1.5863	1.6216
5200			0.0326	0.0531	0.0789	0.0973	0.1119	0.1244	0.1356	0.1458	0.1553	0.1642	0.1728	0.1810	0.1966	0.2114
			845.8	1016.9	1156.0	1240.4	1303.7	1356.6	1403.4	1446.2	1486.3	1524.5	1561.3	1597.2	1666.8	1734.7
			0.9985	1.1370	1.2455	1.3088	1.3545	1.3914	1.4229	1.4509	1.4762	1.4995	1.5214	1.5420	1.5806	1.6161
5400			0.0317	0.0483	0.0728	0.0912	0.1058	0.1182	0.1292	0.1392	0.1485	0.1572	0.1656	0.1736	0.1888	0.2031
			838.5	994.3	1138.1	1227.7	1293.7	1348.4	1396.5	1440.3	1481.1	1519.8	1557.1	1593.4	1663.7	1732.1
			0.9915	1.1175	1.2296	1.2969	1.3446	1.3827	1.4151	1.4437	1.4694	1.4931	1.5153	1.5362	1.5750	1.6109
5600			0.0309	0.0447	0.0672	0.0856	0.1001	0.1124	0.1232	0.1331	0.1422	0.1508	0.1589	0.1667	0.1815	0.1954
			832.4	975.0	1119.9	1214.8	1283.7	1340.2	1389.6	1434.3	1475.9	1515.2	1552.9	1589.6	1660.5	1729.5
			0.9855	1.1008	1.2137	1.2850	1.3348	1.3742	1.4075	1.4366	1.4628	1.4869	1.5093	1.5304	1.5697	1.6058
5800			0.0303	0.0419	0.0622	0.0805	0.0949	0.1070	0.1177	0.1274	0.1363	0.1447	0.1527	0.1603	0.1747	0.1883
			827.3	958.8	1101.8	1201.8	1273.6	1332.0	1382.6	1428.3	1470.6	1510.5	1548.7	1585.8	1657.4	1726.8
			0.9803	1.0867	1.1981	1.2732	1.3250	1.3658	1.3999	1.4297	1.4564	1.4808	1.5035	1.5248	1.5644	1.6008
6000			0.0298	0.0397	0.0579	0.0757	0.0900	0.1020	0.1126	0.1221	0.1309	0.1391	0.1469	0.1544	0.1684	0.1817
			822.9	945.1	1084.6	1188.8	1263.4	1323.6	1375.7	1422.3	1465.4	1505.9	1544.6	1582.0	1654.2	1724.2
			0.9758	1.0746	1.1833	1.2615	1.3154	1.3574	1.3925	1.4229	1.4500	1.4748	1.4978	1.5194	1.5593	1.5960
6500			0.0287	0.0358	0.0495	0.0655	0.0793	0.0909	0.1012	0.1104	0.1188	0.1266	0.1340	0.1411	0.1544	0.1669
			813.9	919.5	1046.7	1156.5	1237.8	1302.7	1358.1	1407.3	1452.2	1494.2	1534.1	1572.5	1646.4	1717.6
			0.9661	1.0515	1.1506	1.2328	1.2917	1.3370	1.3743	1.4064	1.4347	1.4604	1.4841	1.5062	1.5471	1.5844
7000			0.0279	0.0334	0.0438	0.0573	0.0704	0.0816	0.0915	0.1004	0.1085	0.1160	0.1231	0.1298	0.1424	0.1542
			806.9	901.8	1016.5	1124.9	1212.6	1281.7	1340.5	1392.2	1439.1	1482.5	1523.7	1563.1	1638.6	1711.1
			0.9582	1.0350	1.1243	1.2055	1.2689	1.3171	1.3567	1.3904	1.4200	1.4466	1.4710	1.4938	1.5355	1.5735
7500			0.0272	0.0318	0.0399	0.0512	0.0631	0.0737	0.0833	0.0918	0.0996	0.1068	0.1136	0.1200	0.1321	0.1433
			801.3	889.0	992.9	1097.7	1188.3	1261.0	1322.9	1377.2	1426.0	1471.0	1513.3	1553.7	1630.8	1704.6
			0.9514	1.0224	1.1033	1.1818	1.2473	1.2980	1.3397	1.3751	1.4059	1.4335	1.4586	1.4819	1.5245	1.5632
8000			0.0267	0.0306	0.0371	0.0465	0.0571	0.0671	0.0762	0.0845	0.0920	0.0989	0.1054	0.1115	0.1230	0.1338
			796.6	879.1	974.4	1074.3	1155.4	1241.0	1305.5	1362.2	1413.0	1459.6	1503.1	1544.5	1623.1	1698.1
			0.9455	1.0122	1.0864	1.1613	1.2271	1.2798	1.3233	1.3603	1.3924	1.4208	1.4467	1.4705	1.5140	1.5533
8500			0.0262	0.0296	0.0350	0.0429	0.0522	0.0615	0.0701	0.0780	0.0853	0.0919	0.0982	0.1041	0.1151	0.1254
			792.7	871.2	959.8	1054.5	1144.0	1221.9	1288.5	1347.5	1400.2	1448.2	1492.9	1535.3	1615.4	1691.7
			0.9402	1.0037	1.0727	1.1437	1.2084	1.2627	1.3076	1.3460	1.3793	1.4087	1.4352	1.4597	1.5040	1.5439
9000			0.0258	0.0288	0.0335	0.0402	0.0483	0.0568	0.0649	0.0724	0.0794	0.0858	0.0918	0.0975	0.1081	0.1179
			789.3	864.7	948.0	1037.6	1125.4	1204.1	1272.1	1333.0	1387.5	1437.1	1482.9	1526.3	1607.9	1685.3
			0.9354	0.9964	1.0613	1.1285	1.1918	1.2468	1.2926	1.3323	1.3667	1.3970	1.4243	1.4492	1.4944	1.5349
9500			0.0254	0.0282	0.0322	0.0380	0.0451	0.0528	0.0603	0.0675	0.0742	0.0804	0.0862	0.0917	0.1019	0.1113
			786.4	859.2	938.3	1023.4	1108.9	1187.7	1256.6	1318.9	1375.1	1426.1	1473.1	1517.3	1600.4	1679.0
			0.9310	0.9900	1.0516	1.1153	1.1771	1.2320	1.2785	1.3191	1.3546	1.3858	1.4137	1.4392	1.4851	1.5263
10000			0.0251	0.0276	0.0312	0.0362	0.0425	0.0495	0.0565	0.0633	0.0697	0.0757	0.0812	0.0865	0.0963	0.1054
			783.3	854.5	930.2	1011.3	1094.2	1172.6	1242.0	1305.3	1362.9	1415.3	1463.4	1508.6	1593.1	1672.8
			0.9270	0.9842	1.0432	1.1039	1.1638	1.2185	1.2652	1.3065	1.3429	1.3749	1.4035	1.4295	1.4763	1.5180
10500			0.0248	0.0271	0.0303	0.0347	0.0404	0.0467	0.0532	0.0595	0.0656	0.0714	0.0768	0.0818	0.0913	0.1001
			781.5	850.5	923.4	1001.0	1081.3	1158.9	1228.4	1292.4	1351.1	1404.7	1453.9	1500.0	1585.8	1666.7
			0.9232	0.9790	1.0358	1.0939	1.1519	1.2060	1.2529	1.2946	1.3371	1.3644	1.3937	1.4202	1.4677	1.5100

Sh = superheat, F
v = specific volume, cu ft per lb

h = enthalpy, Btu per lb
s = entropy, Btu per R per lb

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Table 3. Superheated Steam - Continued

Abs Press. Lb/Sq In (Sat. Temp.)	Sat Water	Sat Steam	Temperature - Degrees Fahrenheit													
			750	800	850	900	950	1000	1050	1100	1150	1200	1250	1300	1400	1500
11000	v		0.0245	0.0267	0.0296	0.0335	0.0386	0.0443	0.0503	0.0562	0.0620	0.0676	0.0727	0.0776	0.0868	0.0952
	h		739.5	846.9	917.5	992.1	1069.9	1146.3	1215.9	1280.2	1339.7	1394.4	1444.6	1491.5	1578.7	1660.6
	s		0.9196	0.9742	1.0292	1.0851	1.1412	1.1945	1.2444	1.2833	1.3209	1.3544	1.3842	1.4112	1.4595	1.5023
11500	v		0.0243	0.0263	0.0290	0.0325	0.0370	0.0423	0.0478	0.0534	0.0588	0.0641	0.0691	0.0739	0.0827	0.0909
	h		737.7	843.8	912.4	984.5	1059.8	1134.9	1204.5	1268.7	1328.8	1384.4	1435.5	1483.2	1571.8	1654.7
	s		0.9193	0.9698	1.0232	1.0772	1.1316	1.1840	1.2308	1.2727	1.3107	1.3446	1.3750	1.4025	1.4515	1.4949
12000	v		0.0241	0.0260	0.0284	0.0317	0.0357	0.0405	0.0456	0.0508	0.0560	0.0610	0.0659	0.0704	0.0790	0.0869
	h		735.1	841.0	907.9	977.8	1050.9	1124.5	1193.7	1258.0	1318.5	1374.7	1426.6	1475.1	1564.9	1648.8
	s		0.9131	0.9657	1.0177	1.0701	1.1229	1.1742	1.2209	1.2627	1.3010	1.3353	1.3662	1.3941	1.4438	1.4877
12500	v		0.0238	0.0256	0.0279	0.0309	0.0346	0.0390	0.0437	0.0486	0.0535	0.0583	0.0629	0.0673	0.0756	0.0832
	h		732.7	838.6	903.9	971.9	1043.1	1115.2	1184.1	1247.9	1308.8	1365.4	1418.0	1467.2	1558.2	1643.1
	s		0.9101	0.9618	1.0127	1.0637	1.1151	1.1653	1.2117	1.2534	1.2918	1.3264	1.3576	1.3860	1.4363	1.4808
13000	v		0.0236	0.0253	0.0275	0.0302	0.0336	0.0376	0.0420	0.0466	0.0512	0.0558	0.0602	0.0645	0.0725	0.0799
	h		730.3	836.3	900.4	966.8	1036.2	1106.7	1174.8	1238.5	1299.6	1356.5	1409.6	1459.4	1551.6	1637.4
	s		0.9073	0.9582	1.0080	1.0578	1.1079	1.1571	1.2030	1.2445	1.2831	1.3179	1.3494	1.3781	1.4291	1.4741
13500	v		0.0235	0.0251	0.0271	0.0297	0.0328	0.0364	0.0405	0.0448	0.0492	0.0535	0.0577	0.0619	0.0696	0.0768
	h		727.9	834.4	897.2	962.2	1030.0	1099.1	1166.3	1229.7	1291.0	1348.1	1401.5	1451.8	1545.2	1631.9
	s		0.9045	0.9548	1.0037	1.0524	1.1014	1.1495	1.1948	1.2361	1.2749	1.3098	1.3415	1.3705	1.4221	1.4675
14000	v		0.0233	0.0248	0.0267	0.0291	0.0320	0.0354	0.0392	0.0432	0.0474	0.0515	0.0555	0.0595	0.0670	0.0740
	h		725.3	832.6	894.3	958.0	1024.5	1092.3	1158.5	1221.4	1283.0	1340.2	1393.8	1444.4	1538.8	1626.5
	s		0.9019	0.9515	0.9996	1.0473	1.0953	1.1426	1.1872	1.2282	1.2671	1.3021	1.3339	1.3631	1.4153	1.4612
14500	v		0.0231	0.0246	0.0264	0.0287	0.0314	0.0345	0.0380	0.0418	0.0458	0.0496	0.0534	0.0573	0.0646	0.0714
	h		722.8	831.0	891.7	954.3	1019.6	1086.2	1151.4	1213.8	1275.4	1332.9	1386.4	1437.3	1532.6	1621.1
	s		0.8994	0.9484	0.9957	1.0426	1.0897	1.1362	1.1801	1.2208	1.2597	1.2949	1.3266	1.3560	1.4087	1.4551
15000	v		0.0230	0.0244	0.0261	0.0282	0.0308	0.0337	0.0369	0.0405	0.0443	0.0479	0.0516	0.0552	0.0624	0.0690
	h		720.3	829.5	889.3	950.9	1015.1	1080.6	1144.9	1206.8	1268.1	1326.0	1379.4	1430.3	1526.4	1615.9
	s		0.8970	0.9455	0.9920	1.0382	1.0846	1.1302	1.1735	1.2139	1.2525	1.2880	1.3197	1.3491	1.4022	1.4491
15500	v		0.0228	0.0242	0.0258	0.0278	0.0302	0.0329	0.0360	0.0393	0.0429	0.0464	0.0499	0.0534	0.0603	0.0668
	h		717.9	828.2	887.2	947.8	1011.1	1075.7	1139.0	1200.3	1261.1	1319.6	1372.8	1423.6	1520.4	1610.8
	s		0.8945	0.9427	0.9886	1.0340	1.0797	1.1247	1.1674	1.2073	1.2457	1.2815	1.3131	1.3424	1.3959	1.4433

Sh = superheat, F
v = specific volume, cu ft per lb

h = enthalpy, Btu per lb
s = entropy, Btu per R per lb

TO OBTAIN	MULTIPLY	BY
Acres	Sq miles	640.0
Atmospheres	Cm of Hg @ 0 deg C	0.013158
Atmospheres	Ft of H ₂ O @ 39.2 F	0.029499
Atmospheres	Grams/sq cm	0.00096784
Atmospheres	In. Hg @ 32 F	0.033421
Atmospheres	In. H ₂ O @ 39.2 F	0.0024583
Atmospheres	Pounds/sq ft	0.00047254
Atmospheres	Pounds/sq in.	0.068046
Btu	Ft-lb	0.0012854
Btu	Hp-hr	2545.1
Btu	Kg cal.	3.9685
Btu	Kw-hr	3413
Btu	Watt-hr	3.4130
Btu	Kw/hter	96.6506
Btu	Mech. hp	2545.1
Btu	Kw	3413
Btu/(cu ft) (hr)	Tons of refrigeration	12.000
Btu/hr	Watts	3.4127
Btu/hr	Kg cal/kw hr	3.9685
Btu/hr	Cal/(sec) (cm) (deg C)	241.90
Btu/(ft) (ft) (deg F)	Joules/(sec) (cm) (deg C)	5.7803
Btu/(ft) (ft) (deg F)	Cal/(sec) (deg C)	57.803
Btu/(hr) (sq ft)	Cal/(sec) (sq cm)	13.2730
Btu/min	Ft-lb/min	0.0012854
Btu/min	Mech. hp	42.418
Btu/min	Kw	56.896
Btu/lb	Cal/gram	18
Btu/lb	Kg cal/kg	18
Btu/(lb) (deg F)	Cal/(gram) (deg C)	1.0
Btu/(lb) (deg F)	Joules/(gram) (deg C)	0.23889
Btu/sec	Mech. hp	0.70695
Btu/sec	Mech. hp (metric)	0.6971
Btu/sec	Kg cal/hr	0.0011024
Btu/sq ft	Kp cal/sq meter	0.94827
Calories	Ft-lb	0.36867
Calories	Joules	0.32389
Calories	Watt-hr	0.23889
Cal/(cu cm) (sec)	Kw/hter	8640.01
Cal/gram	Btu/lb	0.23888
Cal/(gram) (deg C)	Btu/(lb) (deg F)	0.55556
Cal/(sec) (cm) (deg C)	Btu/(hr) (ft) (deg F)	0.0041336
Cal/(sec) (sq cm)	Btu/(hr) (sq ft)	0.000075341
Cal/(sec) (sq cm) (deg C)	Btu/(hr) (sq ft) (deg F)	0.0001355
Centimeters	Inches	2.540
Centimeters	Microns	0.0001
Cm of Hg @ 0 deg C	Atmospheres	0.007540
Cm of Hg @ 0 deg C	Ft of H ₂ O @ 39.2 F	2.242
Cm of Hg @ 0 deg C	Grams/sq cm	0.07356
Cm of Hg @ 0 deg C	In. of H ₂ O @ 4 C	0.1868

CONVERSION FACTORS

CONVERSION FACTORS — (Continued)

TO OBTAIN	MULTIPLY BY
Cm of Hg @ 0 deg C	Lb/sq in. 5.1715
Cm of Hg @ 0 deg C	Lb/sq ft 0.035913
Cm/deg C	In./deg F 4.5720
Cm/sec	Ft/min 0.508
Cm/sec	Ft/sec 30.48
Cm/(sec) (sec)	Gravity 980.665
Cm of H ₂ O @ 39.2 F	Atmospheres 1033.24
Cm of H ₂ O @ 39.2 F	Lb/sq in. 70.31
Centipoises	Lb/sq in. Density
Centipoises	Ft/sec 1/density
Cu cm	Cu ft 28.317
Cu cm	Cu in. 16.387
Cu cm	Gal. (USA, liq.) 3785.43
Cu cm	Liters 1000.03
Cu cm	Ounces (USA, liq.) 29.573730
Cu cm	Quarts (USA, liq.) 946.358
Cu cm/sec	Cu ft/min 472.0
Cu ft	Cords (wood) 128.0
Cu ft	Cu meters 35.314
Cu ft	Cu yards 27.0
Cu ft	Gal. (USA, liq.) 0.13368
Cu ft	Liters 0.03532
Cu ft/min	Cu meters/sec 2118.9
Cu ft/min	Gal. (USA, liq./sec) 8.0192
Cu ft/lb	Cu meters/kg 16.02
Cu ft/lb	Liters/kg 0.01602
Cu ft/sec	Cu meters/min 0.5886
Cu ft/sec	Gal. (USA, liq./min) 0.0022280
Cu ft/sec	Liters/min 0.0005886
Cu ft/sec	Cu centimeters 0.061023
Cu in.	Gal. (USA, liq.) 231.0
Cu in.	Liters 61.03
Cu in.	Ounces (USA, liq.) 1.805
Cu meters	Cu ft 0.028317
Cu meters	Cu yards 0.7646
Cu meters	Gal. (USA, liq.) 0.0037854
Cu meters	Liters 0.001000028
Cu meters/hr	Gal./min 0.22712
Cu meters/Kg	Cu ft/lb 0.062428
Cu meters/min	Cu ft/min 0.02832
Cu meters/min	Gal./sec 0.22712
Cu meters/sec	Gal./min 0.000063088
Cu yards	Cu meters 1.3079
Dynes	Grams 980.66
Dynes	Pounds (avoir.) 444820.0
Dyne-centimeters	Ft.-lb 13.558,000
Dynes/sq cm	Lb/sq in. 68947
Figs	Joules 10,000,000
Ft	Meters 3.281
Ft of H ₂ O @ 39.2 F	Atmospheres 33.899
Ft of H ₂ O @ 39.2 F	Cm of Hg @ 0 deg C 0.44604

CONVERSION FACTORS — (Continued)

TO OBTAIN	MULTIPLY BY
Ft of H ₂ O @ 39.2 F	In. of Hg @ 32 deg F 1.1330
Ft of H ₂ O @ 39.2 F	Lb/sq ft 0.016018
Ft of H ₂ O @ 39.2 F	Lb/sq in. 2.3066
Ft/min	Cm/sec 1.9685
Ft/min	Miles (USA, statute)/hr 88.0
Ft/sec	Knots 1.6889
Ft/sec	Meters/sec 3.2808
Ft/sec	Miles (USA, statute)/hr 1.4667
Ft/(sec) (sec)	Gravity (sea level) 32.174
Ft/(sec) (sec)	Meters/(sec) (sec) 3.2808
Ft.-lb	Btu 778.0
Ft.-lb	Joules 0.73756
Ft.-lb	Kg.-calories 3087.4
Ft.-lb	Kw-hr 2.655,200
Ft.-lb	Mech. hp-hr 1,980,000
Ft.-lb/min	Btu/min 778.0
Ft.-lb/min	Kg cal/min 3087.4
Ft.-lb/min	Kw 44.254 0
Ft.-lb/min	Mech. hp 33,000
Ft.-lb/sec	Btu/min 12.96
Ft.-lb/sec	Kw 737.56
Ft.-lb/sec	Mech. hp 550.0
Gal. (imperial, liq.)	Gal. (USA, liq.) 0.83268
Gal. (USA, liq.)	Barrels (petroleum, USA) 42
Gal. (USA, liq.)	Cu ft 7.4805
Gal. (USA, liq.)	Cu meters 264.173
Gal. (USA, liq.)	Cu yards 202.2
Gal. (USA, liq.)	Gal. (imperial, liq.) 1.2010
Gal. (USA, liq.)	Liters 0.2642
Gal. (USA, liq.)	Cu ft/sec 448.83
Gal. (USA, liq.)	Cu meters/hr 4.4029
Gal. (USA, liq.)	Cu ft/min 0.12468
Gal. (USA, liq.)/sec	Liters/min 0.0044028
Gal. (USA, liq.)/sec	Grams 15.437
Gal. (USA, liq.)/min	Ounces (avoir.) 437.5
Gal. (USA, liq.)/min	Pounds (avoir.) 7000
Gal. (USA, liq.)/min	Parts/million 0.0584
Gal. (USA, liq.)/min	Grams 0.0648
Gal. (USA, liq.)/min	Ounces (avoir.) 28.350
Gal. (USA, liq.)/min	Pounds (avoir.) 453.5924
Gal./min	Pounds/in. 178.579
Gal./min	Centipoises 0.01
Gal./min	Lb/cu ft 0.016018
Gal./min	Lb/cu in. 27.680
Gal./min	Lb/gal. 0.119826
Gal./min	Ft/(sec) (sec) 0.03108
Gal./min	Centimeters 0.3937
Gal./min	Microns 0.00003937
Gal./min	Atmospheres 24.921
Gal./min	Ft of H ₂ O @ 39.2 F 0.88265
Gal./min	Lb/sq in. 2.0360

CONVERSION FACTORS — (Continued)

TO OBTAIN	MULTIPLY	BY
Inches of Hg @ 32 F	In. of H ₂ O @ 4 C	0.07355
Inches of H ₂ O @ 39.2 F	Lb/sq in.	13.60
Inches/deg F	Cm/deg C	27.673
Joules	Btu	0.21872
Joules	Calories	1054.8
Joules	Ft-lb	4.186
Joules	Kg-meters	1.35582
Joules	Kw-hr	9.807
Joules	Mech. hp-hr	3.600,000
Joules	Pounds (avoird.)	2.684,500
Kg cal	Btu	0.45359
Kg cal	Ft-lb	0.2520
Kg cal	Joules	0.00032389
Kg cal	Kw-hr	0.0002389
Kg cal	Mech. hp-hr	860.01
Kg cal/kg	Btu/lb	641.3
Kg cal/kw-hr	Btu/kw-hr	0.5556
Kg cal/min	Ft-lb/min	0.2520
Kg cal/min	Kw	0.0003239
Kg cal/min	Mech. hp	14.33
Kg cal/sq meter	Btu/sq ft	10.70
Kg/cu meter	Lb/cu ft	2.712
Kg/(hr) (metric)	Centipoises	16.018
Kg/hter	Lb/pal (USA, liq)	3.60
Kg/meter	Lb/ft	0.11983
Kg/sq cm	Atmospheres	1.488
Kg/sq cm	Lb/sq in.	1.0332
Kg/sq meter	Lb/sq ft	0.0703
Kg/sq meter	Lb/sq in.	4.8824
Km	Miles (USA, statute)	703.07
Kw	Btu/min	1.6093
Kw	Ft-lb/min	0.01758
Kw	Ft-lb/sec	0.00002259
Kw	Kg cal/hr	0.00135582
Kw	Kg cal/min	0.0011628
Kw	Mech. hp	0.069767
Kw-hr	Btu	0.7457
Kw-hr	Ft-lb	0.0000293
Kw-hr	Kp cal	0.000003766
Kw-hr	Mech. hp-hr	0.0011628
Knobs	Ft/sec	0.7457
Knobs	Miles/hr	0.5921
Liters	Cu ft	0.8684
Liters	Cu in.	28.316
Liters	Cu centimeters	0.01639
Liters	Gal. (imperial, liq)	999.973
Liters	Gal. (USA, liq)	4.546
Liters/kg	Gal. (USA, liq)	3.78533
Liters/min	Cu ft/sec	62.42621
Liters/min	Gal. (USA, liq)/min	1.699.3
Liters/min	Gal. (USA, liq)/min	3.785

CONVERSION FACTORS — (Continued)

TO OBTAIN	MULTIPLY	BY
Liters/sec	Cu ft/min	0.47193
Liters/sec	Gal/min	0.063088
Mech. hp	Btu/hr	0.063088
Mech. hp	Btu/min	0.0003929
Mech. hp	Ft-lb/sec	0.023575
Mech. hp	Kg cal/min	0.0018182
Mech. hp	Kw	0.093557
Mech. hp-hr	Btu	1.3410
Mech. hp-hr	Ft-lb	0.00039292
Mech. hp-hr	Kg-calories	0.0000050505
Mech. hp-hr	Kw-hr	0.0015593
Mech. hp-hr	Feel	1.3410
Meters	Inches	0.3048
Meters	Miles (intl., nautical)	0.0254
Meters	Miles (USA, statute)	1.852.0
Meters	Miles (USA, statute)	1.609.344
Meters	Ft/min	0.3048
Meters/min	Ft/min	0.3048
Meters/min	Ft/sec	26.82
Meters/sec	Ft/sec	0.3048
Meters/sec	Kn/hr	0.2778
Meters/sec	Kn/s	0.5148
Meters/sec	Miles (USA, statute)/hr	0.44704
Meters/sec	Ft/sec (sec)	0.3048
Meters/sec	Inches	25.400
Meters/sec	Mils	25.4
Meters	Km	0.54
Meters (intl., nautical)	Miles (USA, statute)	0.8670
Meters (intl., nautical)	Knobs	1.0
Meters (USA, statute)	Km	0.6214
Meters (USA, statute)	Miles (intl., nautical)	1.151
Meters (USA, statute)	Knobs	1.151
Meters	Ft/min	0.011664
Meters	Ft/sec	0.68182
Meters/min	Meters/min	0.01728
Meters/sec	Meters/sec	2.2369
Cm ft/lb	Cm ft/lb	62.42621
Centimeters	Meters	0.001
Centimeters	Inches	39.37
Centimeters	Meters	1000
Centimeters	Radians	0.05937
Centimeters	Grains (avoir)	313.75
Centimeters	Grains	0.0022857
Centimeters	Gal. (USA, liq)	0.035274
Centimeters	Gal./pal (USA, liq)	128.0
Centimeters	Ft/100 ft	17.118
Centimeters	Grains	1.0
Centimeters	Grains	0.0001429
Centimeters	Grains	0.0022046
Centimeters	Kp	2.2046
Centimeters	Tons, long	2240
Centimeters	Tons, metric	2204.6

CONVERSION FACTORS—(Continued)

TO OBTAIN	MULTIPLY	BY
Pounds (avoird.)		2000
Pounds/cu ft		62.428
Pounds/cu ft		0.062428
Pounds/cu ft		7.48
Pounds/cu in.		0.036127
Pounds/ft		0.67197
Pounds/hr		132.28
Pounds/(hr) (11)		2.42
Pounds/inch		0.0056
Pounds/(sec) (11)		0.000672
Pounds/sq inch		14.696
Pounds/sq inch		0.19337
Pounds/sq inch		0.43352
Pounds/sq inch		0.491
Pounds/sq inch		0.0361
Pounds/sq inch		14.223
Pounds/sq inch		0.0014223
Pounds/gal. (USA, liq)		8.3452
Pounds/gal. (USA, liq)		0.1337
Quarts (USA, liq)		231
Quarts (USA, liq)		0.0010567
Quarts (USA, liq)		0.01732
Quarts (USA, liq)		1.057
Sq centimeters		929.0
Sq ft		6.4516
Sq ft		43.560
Sq inches		10.764
Sq meters		0.155
Sq meters		4046.9
Sq meters		0.0929
Sq miles (USA, statute)		0.001562
Sq miles		155.000
Sq miles		1,000,000
Tons (metric)		0.9072
Tons (short)		1.1023
Tons (short)		1054.8
Watts		1.0936
Yards		
Tons, short		
Grams/cu cm		
Kg/cu meter		
Pounds/gal.		
Grams/cu cm		
Kg/meter		
Kg/min		
Centipoises		
Grams/cm		
Centipoises		
Atmospheres		
Cm of Hg @ 0 deg C		
Ft of H ₂ O @ 39.2 F		
In. Hg @ 32 F		
In. H ₂ O @ 39.2 F		
Kg/sq cm		
Kg/sq meter		
Kg/liter		
Pounds/cu ft		
Pounds/cu inch		
Cu cm		
Cu in.		
Liters		
Sq ft		
Sq inches		
Acres		
Sq meters		
Sq centimeters		
Acres		
Sq ft		
Acres		
Sq cm		
Sq inches		
Tons (short)		
Tons (metric)		
Bit/sec		
Meters		