1. Consider this simple model for a bivalent ligand-monovalent receptor interaction.



(a) Derive time-dependent governing equations for C_1 , C_2 , and C_3 as a function of R_T , L, and rate constants. Assume no ligand depletion.

(b) Rearrange solutions in (i) to obtain governing equations for singly occupied receptors ($C_s = C_1 + C_3$) and cross-linked receptors ($C_x = C_2$) as a function of R_T , L, C_s , C_x and rate constants.

2. (a)For the aortic valve of a human being fully open, describe the nature of the flow field both in words and using a sketch. Also, describe the process by which the aortic valve closes.

(b) Describe how you would analyze differences in aortic flow in a mouse as compared to that in a human.

3. The femur (thigh bone) consists of an outer shell of compact bone and an inner region of spongy bone. A man is standing on one foot and holding a heavy package. We can determine from experiment the following: the radius of the spongy region is r_s , the outer radius of the femur is r_c , the modulus of elasticity for the spongy bone is E_s , the modulus of elasticity for the compact bone is E_c , and the weight of the man and the package together is W.

(a) Find a relation for the stresses in the different regions of the femur in terms of r_s , r_c , E_s , E_c , and W. Is there a ratio of $E_s : E_c$ at which the contribution of the spongy bone toward the overall stress may be neglected?

(b) Assume next, that the man twists his body and applies a torque T on his femur. We can experimentally determine that the spongy bone has a shear modulus G_s and compact bone has a shear modulus G_c . What is the shear stress, $\sigma_{\theta z}$, in the spongy bone and the compact bone. Is there a ratio of $G_s: G_c$ at which the contribution of spongy bone toward the overall shear stress may be neglected?

(c) While the man is standing on one foot and twisting, assuming a state of plane stress at the outer surface of the bone (in the θ - z plane), what is the direction of the principal stresses? What the direction of maximum shear stress?

Axial Extension of a Rod

$$\sigma_{zz} = \frac{f}{A}$$

$$u_{z}(z = b) - u_{z}(z = a) = \int_{z=a}^{z=b} \frac{f(z)}{A(z)E(z)}$$
Torsion of a rod or tube
$$\sigma_{z\theta} = \frac{Tr}{J}$$

$$\Theta(z = b) - \Theta(z = a) = \int_{z=a}^{z=b} \frac{T(z)}{J(z)G(z)} dz$$

$$J = \frac{\pi c^{4}}{2} \text{ (for solid cylinder)}$$

$$J = \frac{\pi (c^{4} - d^{4})}{2} \text{ (for hollow cylinder)}$$

Stress transformation equations for plane stress (in x-y plane)

$$\sigma_{x'x'} = \sigma_{xx} \cos^2 \alpha + 2\sigma_{xy} \sin \alpha \, \cos \alpha + \sigma_{yy} \sin^2 \alpha = \frac{\sigma_{xx} + \sigma_{yy}}{2} + \frac{\sigma_{xx} - \sigma_{yy}}{2} \cos 2\alpha + \sigma_{xy} \sin 2\alpha$$

$$\sigma_{y'y'} = \sigma_{xx} \sin^2 \alpha - 2\sigma_{xy} \sin \alpha \, \cos \alpha + \sigma_{yy} \cos^2 \alpha = \frac{\sigma_{xx} + \sigma_{yy}}{2} + \frac{\sigma_{yy} - \sigma_{xx}}{2} \cos 2\alpha - \sigma_{xy} \sin 2\alpha$$

$$\sigma_{x'y'} = \sigma_{y'x'} = 2\left(\frac{\sigma_{yy} - \sigma_{xx}}{2}\right) \sin \alpha \, \cos \alpha + \sigma_{x'y'} \left(\cos^2 \alpha - \sin^2 \alpha\right) = \frac{\sigma_{yy} - \sigma_{xx}}{2} \sin 2\alpha + \sigma_{xy} \cos 2\alpha$$

$$\alpha_{p} = \frac{1}{2} \tan^{-1} \left[\frac{2\sigma_{xy}}{\sigma_{xx} - \sigma_{yy}}\right]$$

$$\alpha_{s} = \frac{1}{2} \tan^{-1} \left[\frac{\sigma_{yy} - \sigma_{xx}}{2}\right]$$

Here σ_{ij} denotes the components of stress, $u_z(z)$ is the displacement at location z along the axis of the rod, A(z) is the cross sectional area of the rod at z, E(z) is the elastic modulus at z, J(z) is the second polar moment of area at z, $\Theta(z)$ is the angle of twist at z, G(z) is the shear modulus at z, c is the outer radius for the rod/tube, d is the inner radius of a tube, α denotes the angle between the x and x' coordinate axes, α_p is the angle of principal direction, and α_s is the angle of maximum shear stress.