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GEORGIA INSTITUTE OF TECHNOLOGY

The George W. Woodruff
School of Mechanical Engineering

Ph.D. Qualifiers Exam - Fall Semester 1999

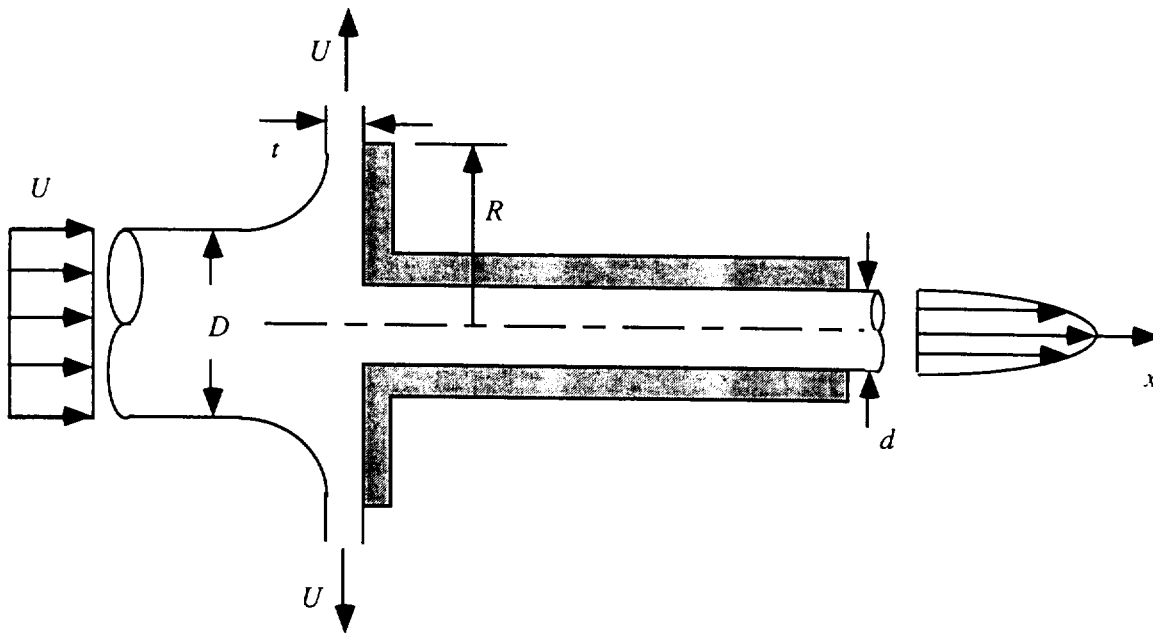
Fluid Mechanics

EXAM AREA

Assigned Number (DO NOT SIGN YOUR NAME)

- Please sign your name on the back of this page—

WORK ALL PROBLEMS—ALL PROBLEMS ARE OF EQUAL WEIGHT



1. A flange of exterior diameter $2R$ is attached to a tube of inside diameter d . A jet of water of diameter D approaches the flange with uniform speed U . The flange deflects a portion of the jet into an axisymmetric sheet of thickness t at the point where it leaves the flange with negligible change in speed. The remainder of the water passes through the tube, developing into a laminar parabolic velocity profile of the form

$$u(r) = \frac{3}{2}U \left(1 - \frac{4r^2}{d^2} \right),$$

where the maximum speed at the centerline is $3/2$ the speed of the approaching flow.

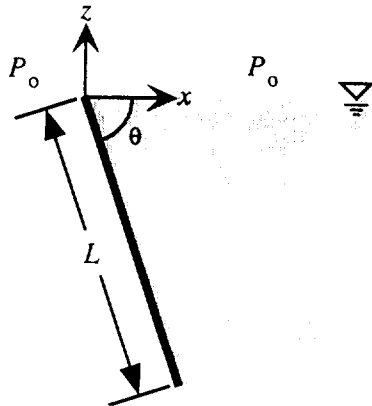
- If half of the mass of the incoming jet is deflected by the flange, determine both the sheet thickness t and the diameter d necessary to accomplish this.
- For the case considered in part a, determine the force required to hold the flange and tube in place.

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2. Consider a liquid where compressibility effects are significant. The simplest model for a compressible liquid assumes a constant sound speed in the liquid a . Pressure P and density ρ variations are then described by the following relation:

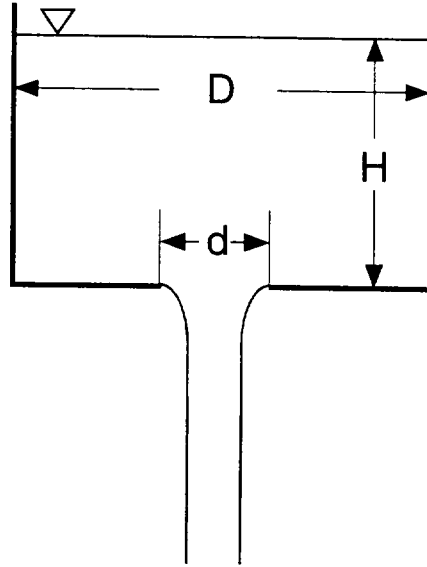
$$dP = a^2 d\rho.$$

- a. Find the density and pressure distributions, $\rho(z)$ and $P(z)$, respectively, in a compressible liquid as a function of depth z , given $\rho(0) = \rho_0$ and $P(0) = P_0$.
- b. Find the net force per unit width due to this pressure distribution on a flat plate of length L and angle of inclination θ immersed in a compressible liquid with its top edge at the free surface ($z = 0$), as shown below. Please give net force in terms of its horizontal (x) and vertical (z) components. Note that there is compressible liquid only on one side of the plate; the pressure on the other side is P_0 .

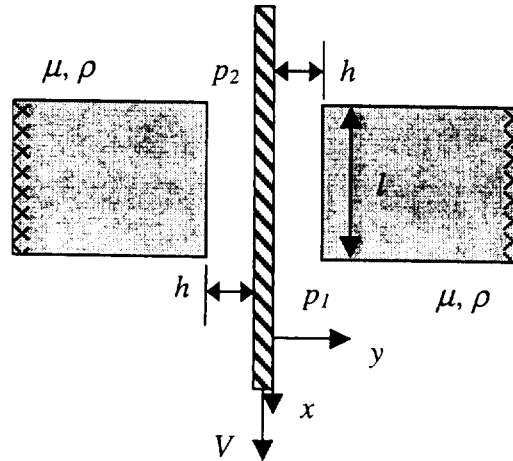


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3. The liquid in the cylindrical storage tank shown below is drained through a small round orifice ($d/D \ll 1$) at the bottom. It is desired to design a small-scale model of the system to measure the change in liquid level ΔH .



- Using dimensional analysis, determine ΔH as a function of the other dimensionless parameters.
- How does the drain time in the model scale relative to the prototype?
- If viscous effects can be neglected, can the same fluid be used for the model and prototype? Explain.

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4. A long vertical plate (hatched) is being pulled at a steady velocity V through a slit in a horizontal plate (light gray) as shown in the figure below. An incompressible liquid of density ρ and viscosity μ flows through the gap between the two plates driven by the motion of the vertical plate and a pressure change from the bottom to the top of the horizontal plate $\Delta p = p_1 - p_2$. The gap width h on each side of the vertical plate is much smaller than the length l of the gap. Assuming two-dimensional flow and ignoring gravity, find the following:
- the magnitude and *sign* of the pressure change along the gap so that the net mass flux through the gap is zero, and
 - the magnitude and *direction* of the force per unit width exerted by the fluid on the vertical plate.

The two-dimensional Navier-Stokes equations and the continuity equation are

$$\rho \left\{ \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right\} = -\frac{\partial p}{\partial x} + \rho g_x + \mu \left\{ \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right\}$$

$$\rho \left\{ \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right\} = -\frac{\partial p}{\partial y} + \rho g_y + \mu \left\{ \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right\}$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$